

Mechanics of plant root pullout from soil

(M. Kinoshita, T. Yamaguchi, in preparation.)

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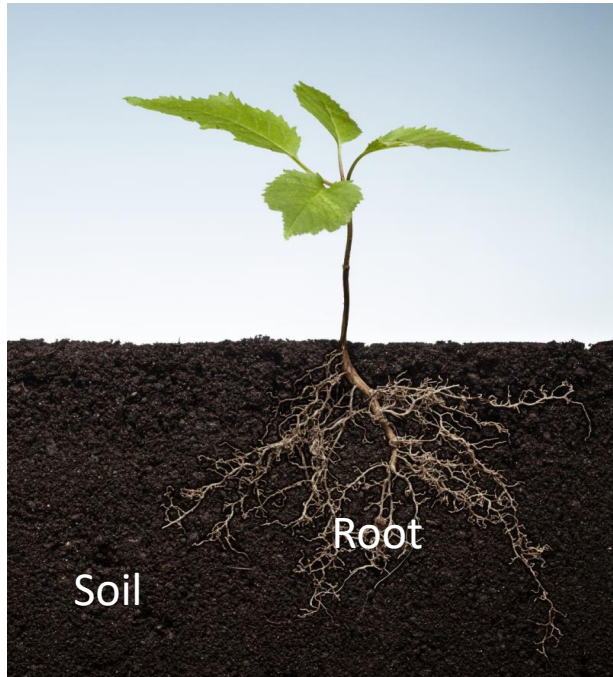
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新学術領域研究
(複合)



Background: Mechanical functions of plant roots



Functions of plant roots

- Adsorption of water and nutrients
- Storage of carbohydrates
- Support of plant's body
- Strengthening and Toughening of soil

Question:

How do plant roots support their bodies and toughen soil?



Landslide



Lodging of trees

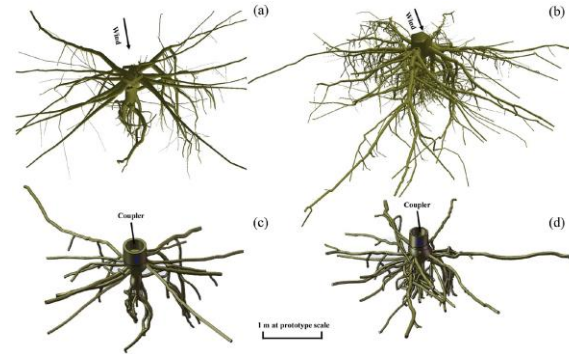
Plant-Soil interactions are one of the most important topics in

- Forest Science
- Crop Science
- Geoscience
- Civil Engineering

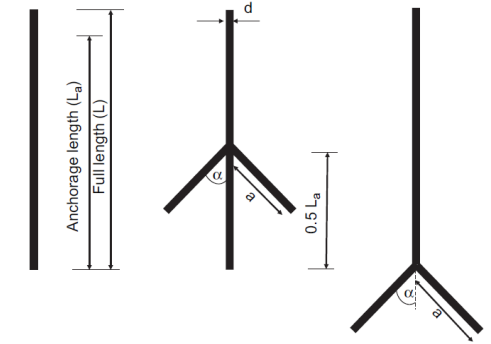
Background: Previous studies on root mechanics

Experiment

- Force-Displacement characteristics
- Geometrical factors
- Model root



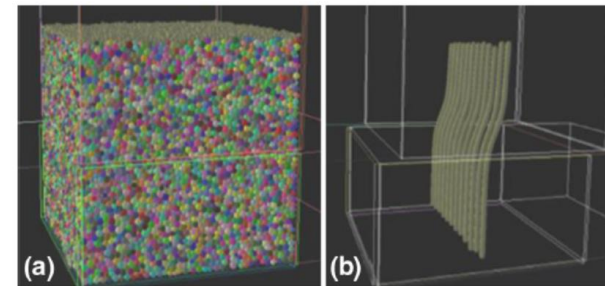
X. Zhang et al., Plant Soil 456:289-305 (2020)



S. B. Mickovski et al., Eur. J. Soil Sci. **58**, 1471 (2007)

Mechanical/mathematical modeling

- Soil mechanics + Simple root geometry
- FEM/DEM simulations
- Root Bundle Model



Z. Mao, M. Yang, F. Bourrier, T. Fourcaud, Plant Soil **381**, 249 (2014)

However,

- Details on **structure-soil interactions**
- Effect of **geometry and elasticity of roots**
- **Theoretical features**

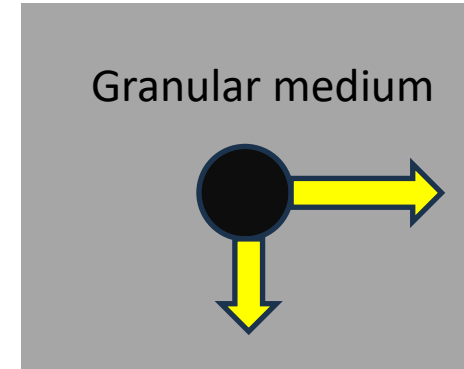
have been poorly understood.

Background: Granular physics viewpoint

Resistance force acting on granular matter

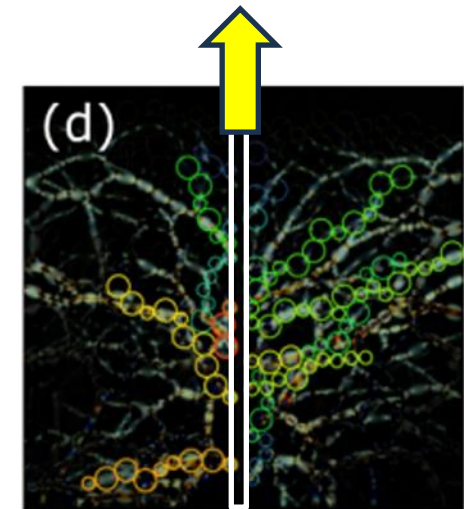
Cylindrical/Spherical object in steady motion

T. A. Brzinski et al., Phys. Rev. Lett. 111, 168002 (2013)



2D photoelasticity experiment during pullout of a rod

F. Okubo, H. Katsuragi, Modern Phys. Lett. (2020)



F. Okubo, H. Katsuragi, Modern Physics Letters B, (2020).

Objectives

- To investigate the effects of root structure and elasticity on the pull-out behavior.
- To elucidate the mechanisms in a quantitative manner.

Approaches

- Pullout experiments with systematic parameter change
- Theoretical description



A “Digged-out” tree root
(at Hokkaido University forest)

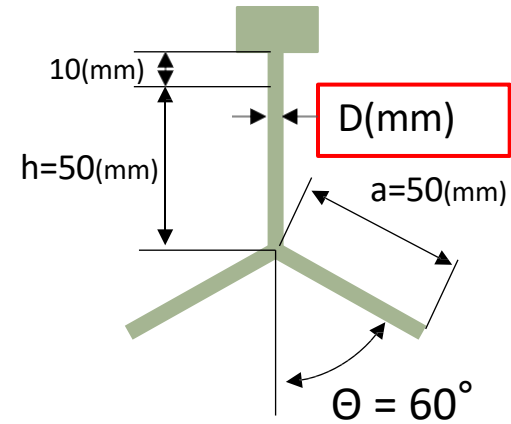
Pull-out experiment

- Root → **3D printed model**

Fabricated with 3D printer (Form3, Formlabs)

Material: Resin ($E = 808 \text{ MPa}$), Rubber ($E = 25.5 \text{ MPa}$)

Diameter: $D = 1, 1.5, 2, 3, 4, 5, 6, 7, 8 \text{ (mm)}$



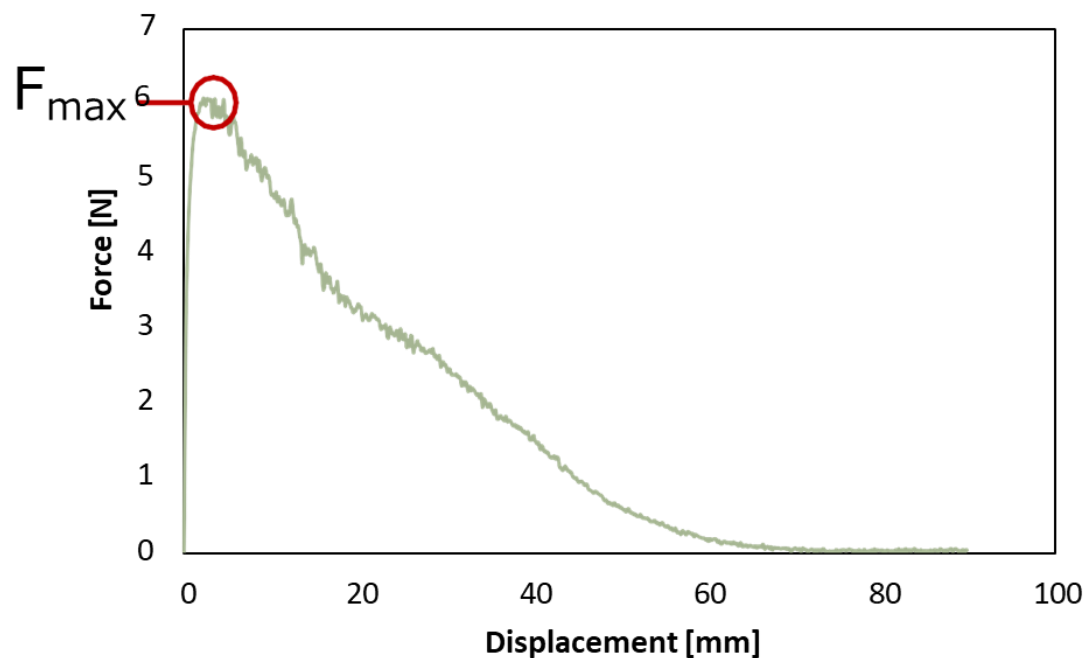
- Soil → **Glass beads**

We mixed beads with three different sizes (0.2, 0.5, 1 mm) by 1:1:1 (in volume)

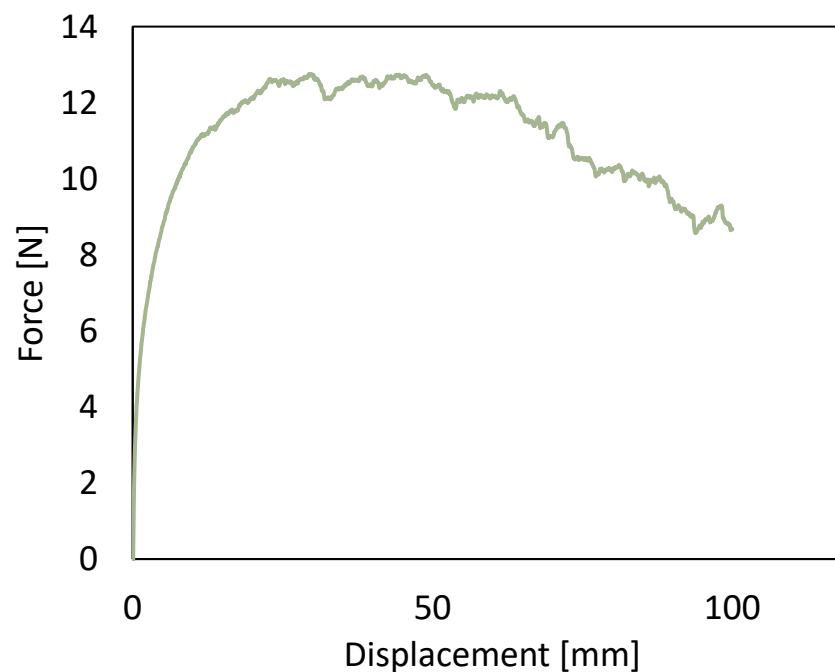


Pull-out behavior for our model and actual plants

3D-printed model root



Actual Plant root

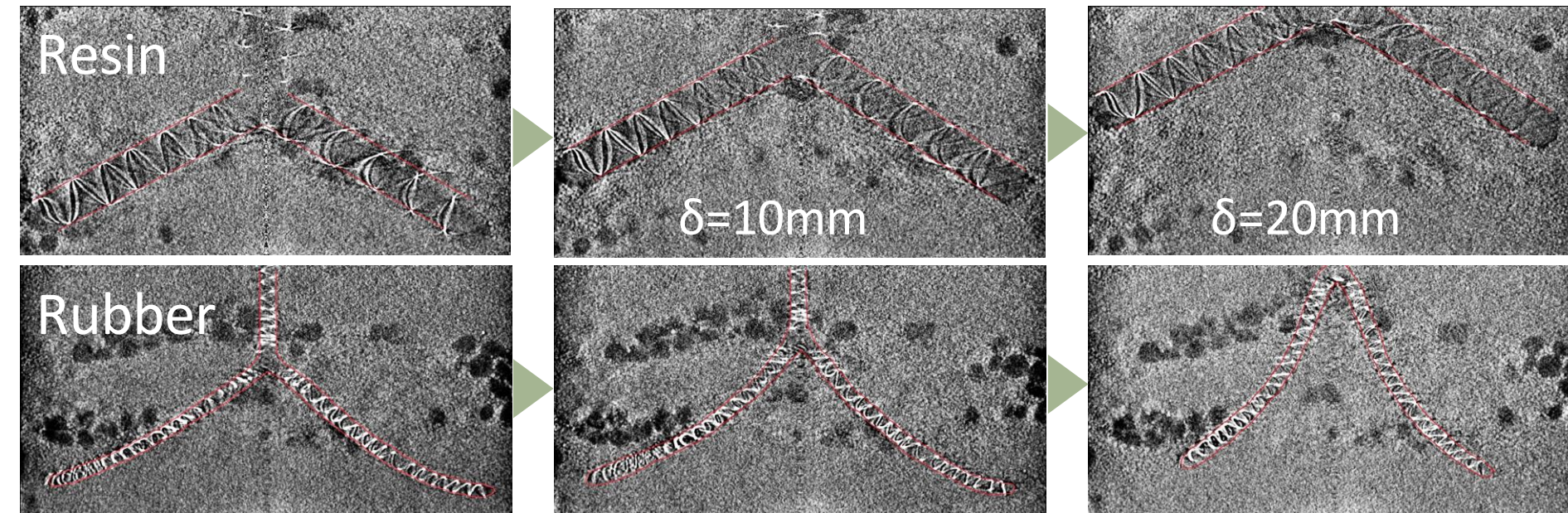


Ardisia crenata
(マンリョウ)

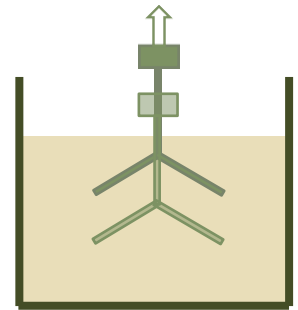
After reaching F_{\max} at small displacement, monotonic decrease was observed for both 3D-printed model and actual plant.

Results: Pull-out behavior

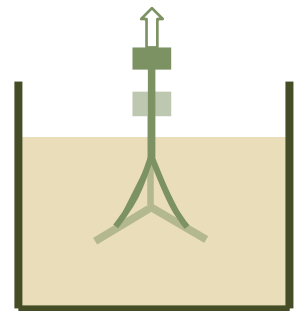
X-ray CT image



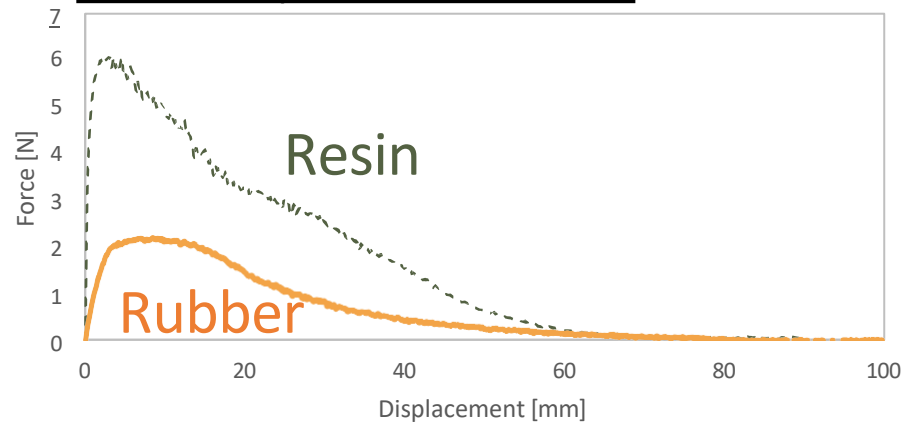
Resin \rightarrow Keep its original shape



Rubber \rightarrow Shrink



Force-Displacement curve



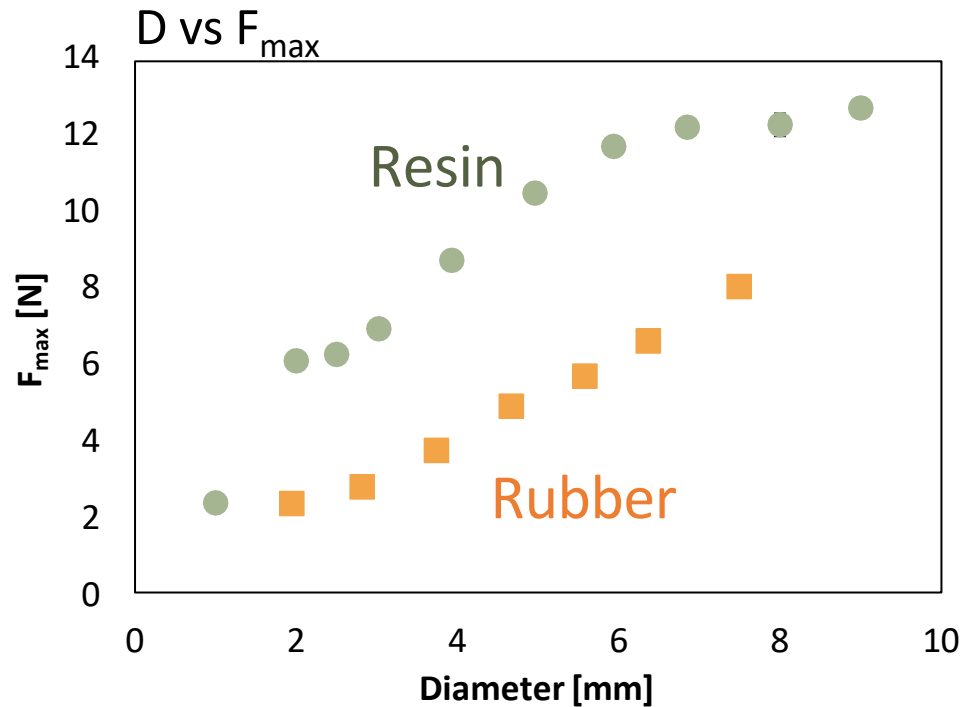
A factor to determine the maximum force

Bending rigidity ($= EI = E \frac{\pi}{64} D^4$)

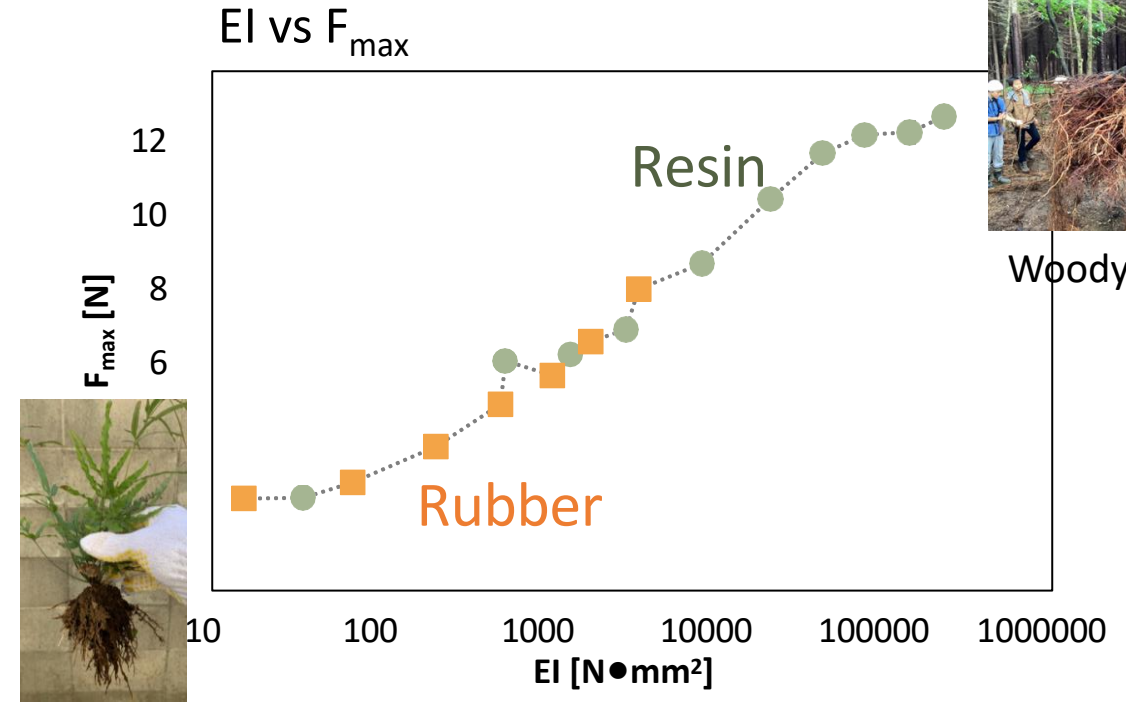
E: Young's modulus

I : 2nd moment of cross-section

D: Diameter



Different trends appear



Herbaceous plant

A “master curve” is obtained



Woody plant

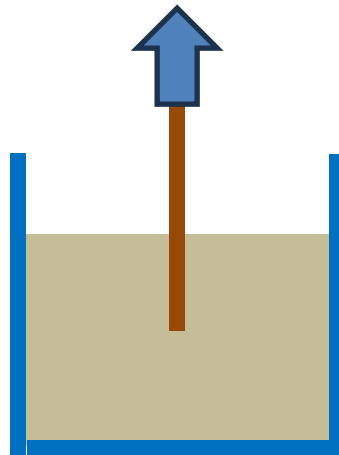
Description with theoretical models

To calculate the maximum force **step by step**

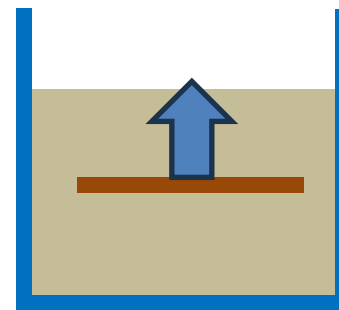
Step 1: Vertical root

Step 2: Horizontal root

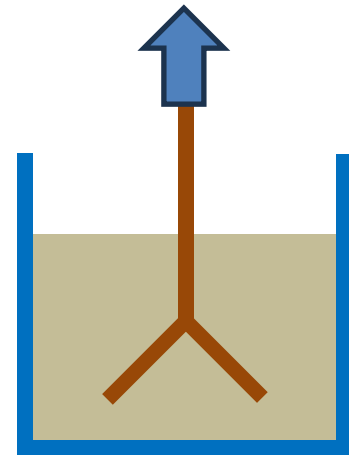
Step 3: Branched root



Vertical root



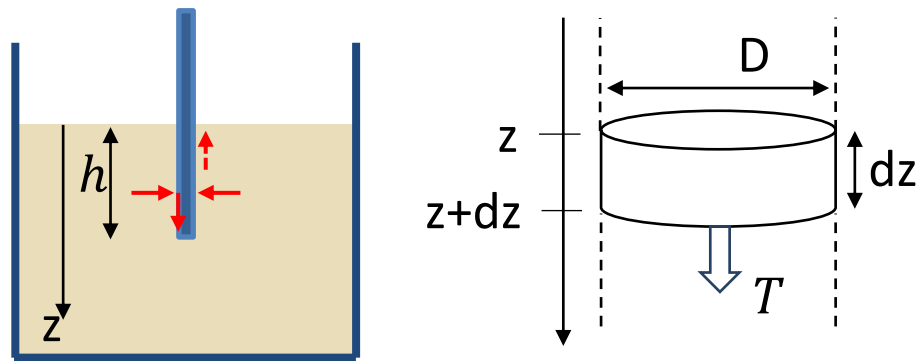
Horizontal root



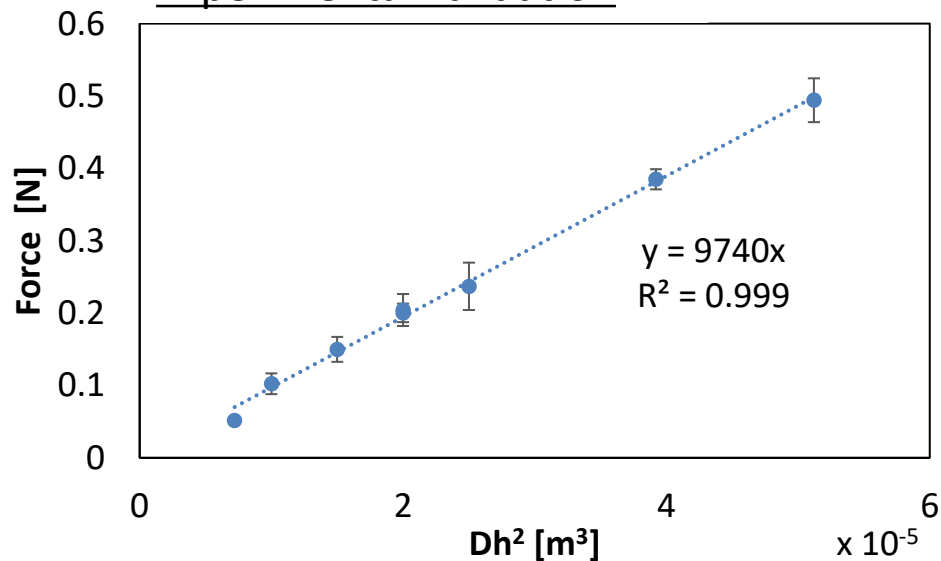
Branched root

Theory 1: Vertical root

Pullout of a smooth tap root → **Friction**



Experimental validation



- Lateral stress at depth z (Janssen's formula)
 $\sigma(z) = K\rho g z$ ρ : Density, g : Gravity constant
 K : Lateral pressure coefficient
- Frictional stress
 $\tau(z) = \mu_{max}\sigma(z)$ μ_{max} : Maximum friction coefficient
 (cf. $F_{max} = \mu_{max}F_N$)
- Maximum force

$$F_{tap} = \frac{K\rho g \pi \mu_{max}}{2} Dh^2 \quad F_{tap} \propto D, h^2$$



$F_{tap} \propto D, h^2$ is reasonable

Theory 2: Horizontal root

Tracking particle motions of glass beads during pull-out

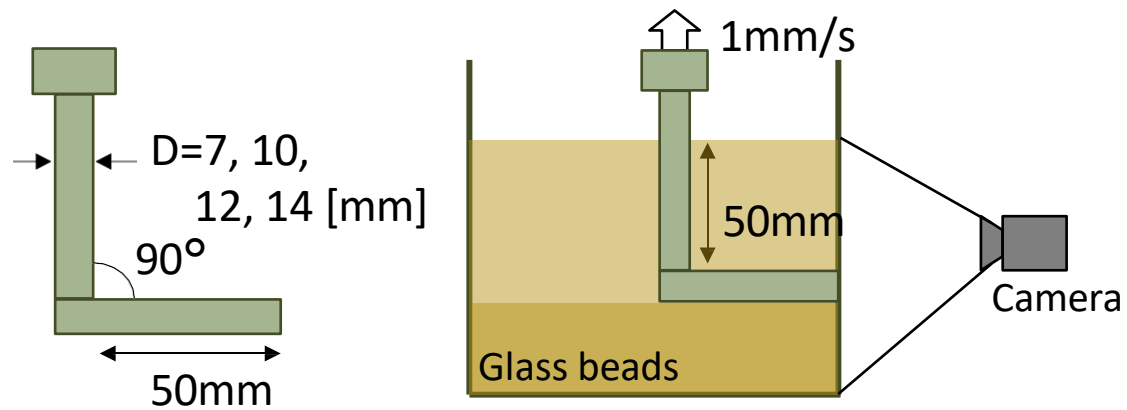
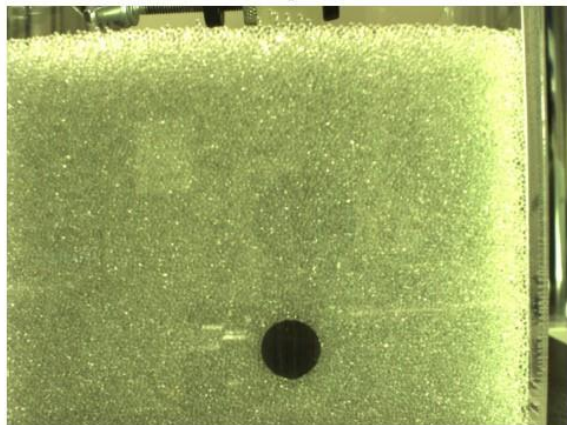
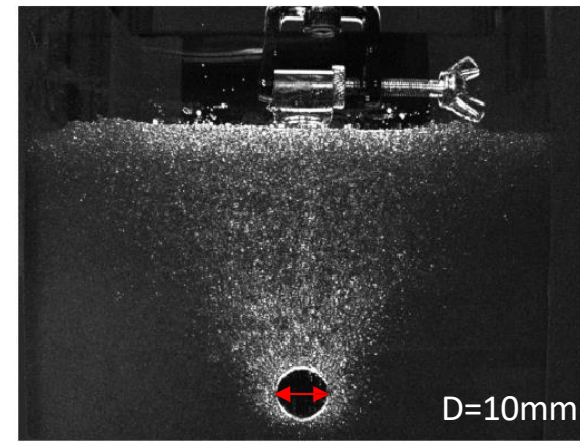


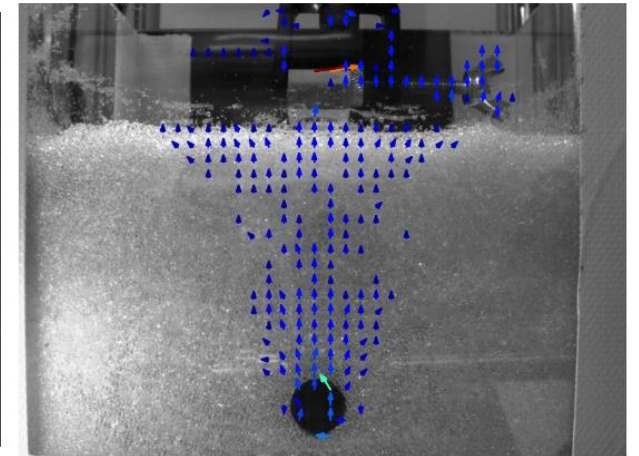
Image 1



Extracting particle motions around the force peak

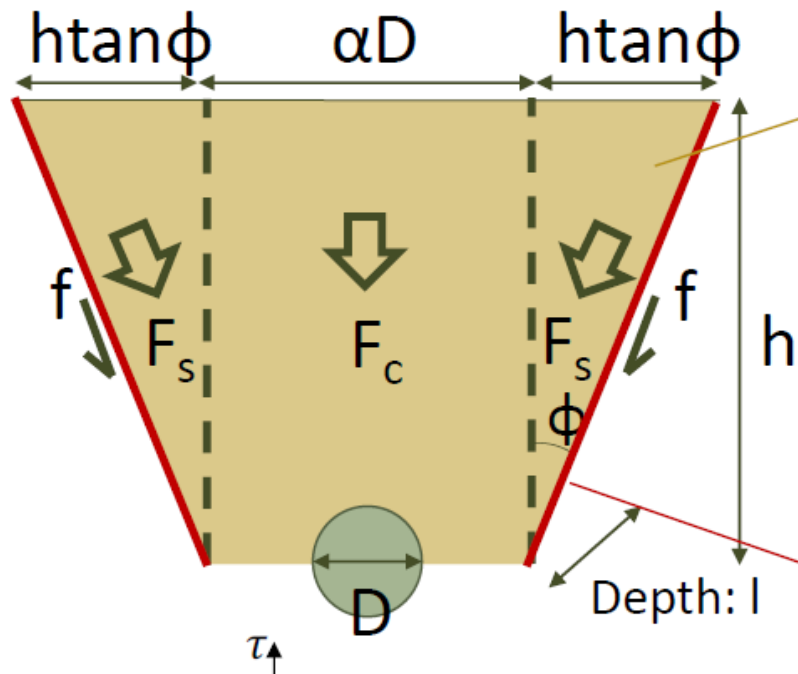


Subtraction of two consecutive images



Displacement vector

Theory 2: Horizontal root



Weight of glass beads in the trapezoidal region

$$F_c \text{ (中央の長方形部分)} = \rho g \alpha D h l$$

$$F_s \text{ (両サイドの三角形部分)} = 2 \rho g \cdot \frac{1}{2} h^2 l \tan \phi \cdot \cos \phi$$

$$= \rho g h^2 l \sin \phi$$

ϕ : Internal friction angle

Friction force on the shear plane

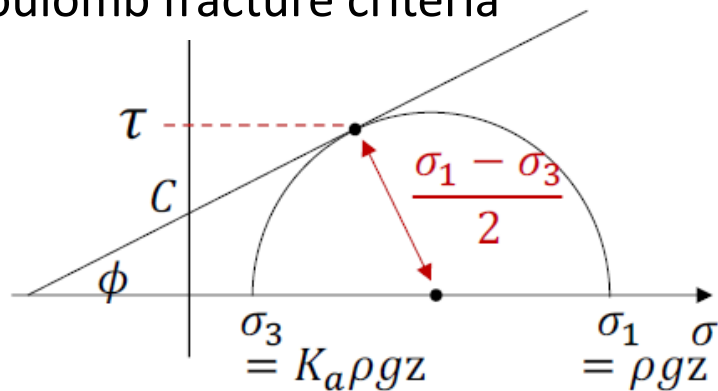
Friction stress at depth z

$$\tau = \frac{1 - K_a}{2} \rho g z \cos \phi \quad K_a: \text{主動粉体圧係数}$$

Total friction force

$$f = \frac{1 - K_a}{2} \rho g h^2 l \cos \phi$$

Mohr-Coulomb fracture criteria



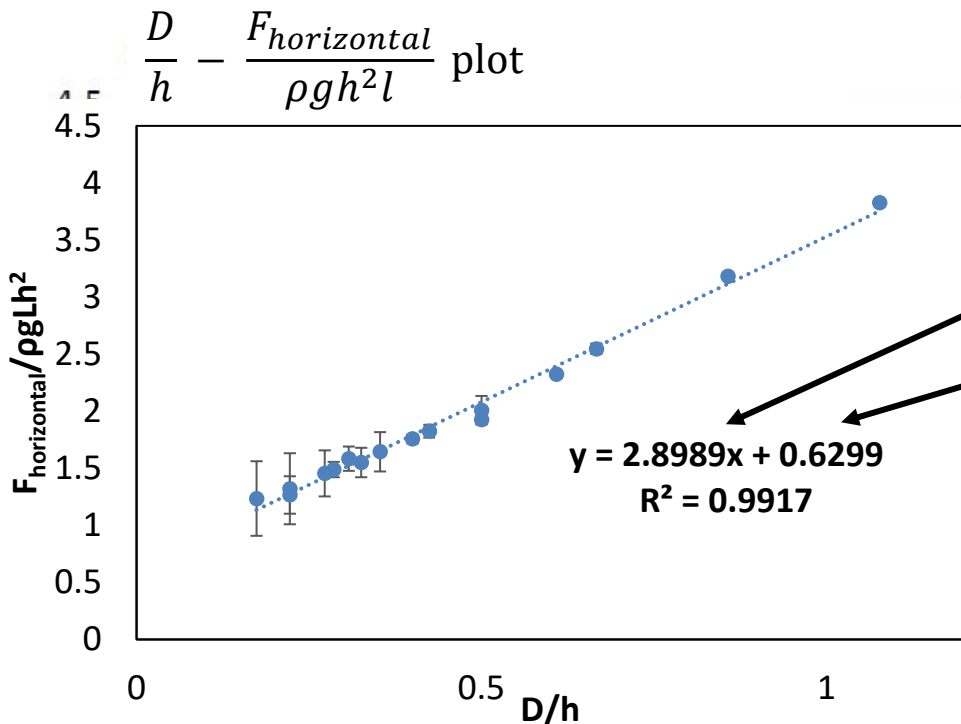
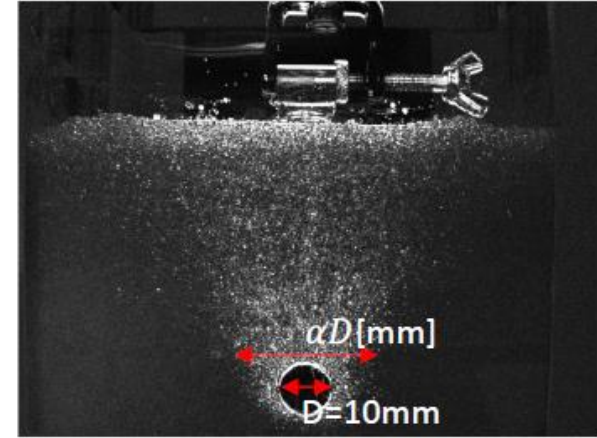
Theory 2: Horizontal root

- Total force in the horizontal root

$$F_{horizontal} = F_c + (F_s + f) \cos \phi$$

$$= \rho g h^2 l \left\{ \alpha \frac{D}{h} + \cos \phi \left(\sin \phi + \frac{1-K_a}{2} \cos \phi \right) \right\}$$

$$\frac{F_{horizontal}}{\rho g h^2 l} = \alpha \frac{D}{h} + \cos \phi \left(\sin \phi + \frac{1-K_a}{2} \cos \phi \right)$$



$$\phi = 26 [^\circ]$$

$$\frac{F_{horizontal}}{\rho g h^2 l} = \alpha \frac{D}{h} + 0.64$$

$\frac{1}{2 \sim 3}$

$$\alpha = 2.90$$

$$\cos \phi \left(\sin \phi + \frac{1-K_a}{2} \cos \phi \right) = 0.63$$

$$\frac{F_{horizontal}}{\rho g h^2 l} = 2.9 \frac{D}{h} + 0.63$$

Good agreement

Theory 3: Branched root in the flexible and rigid limits

- Flexible limit

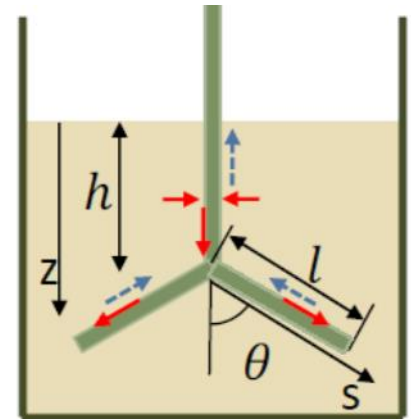
Pullout with pure sliding
(No fracture of soil)

➤ Friction force on the lateral roots

$$F_{lat_fri} = \rho g \pi \mu_{max} D \left(\frac{1+K}{2} + \frac{1-K}{2} \cos 2\theta \right) \left(hl + \frac{\cos \theta}{2} l^2 \right)$$

➤ Total pull-out force

$$F_{flexible} = F_{tap} + 4F_{lat_fri} = \rho g \pi \mu_{max} D \left[\frac{1}{2} K h^2 + \{ (1+K) + (1-K) \cos 2\theta \} (2hl + l^2 \cos \theta) \right]$$



Theory 3: Branched root in the flexible and rigid limits

- Rigid limit

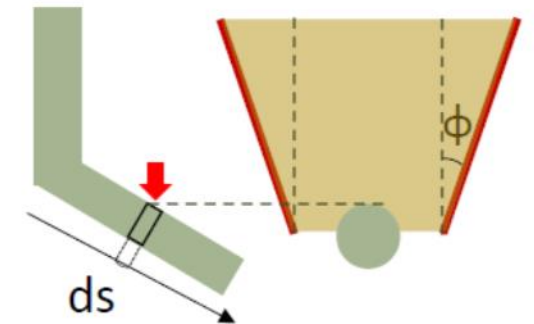
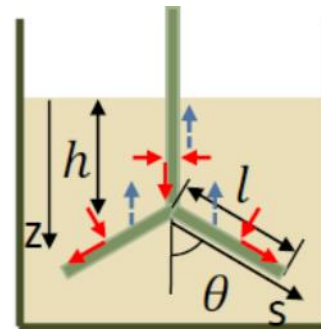
Pullout with soil fracture

- Fracture resistance from soil

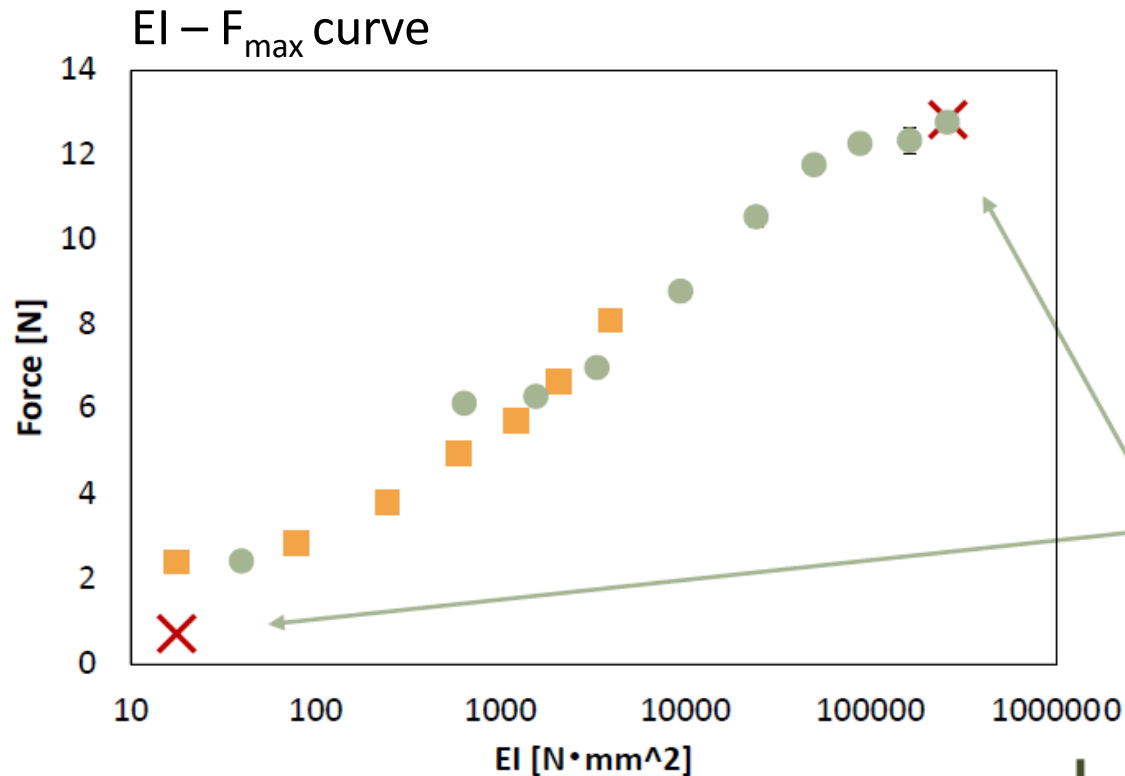
$$F_{lat_res} = \rho g l \sin \theta \left\{ \alpha D \left(h + \frac{\cos \theta}{2} l \right) + \cos \phi \left(\sin \phi + \frac{1 - K_a}{2} \cos \phi \right) \left(h^2 + h l \cos \theta + \frac{1}{3} l^2 \cos^2 \theta \right) \right\}$$

- Total pull-out force

$$F_{stiff} = F_{tap} + 4(F_{lat_fri} \cos \theta + F_{lat_res})$$



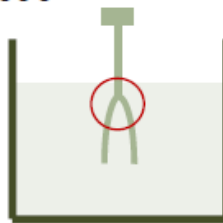
Theory 3: Comparison with experiment



Input Parameters

$$\rho = 1.60 \text{ g/cm}^3, K\mu_{max} = 0.39,$$
$$h = l = 5.0 \times 10^{-2} \text{ m}, \theta = \pi/3$$

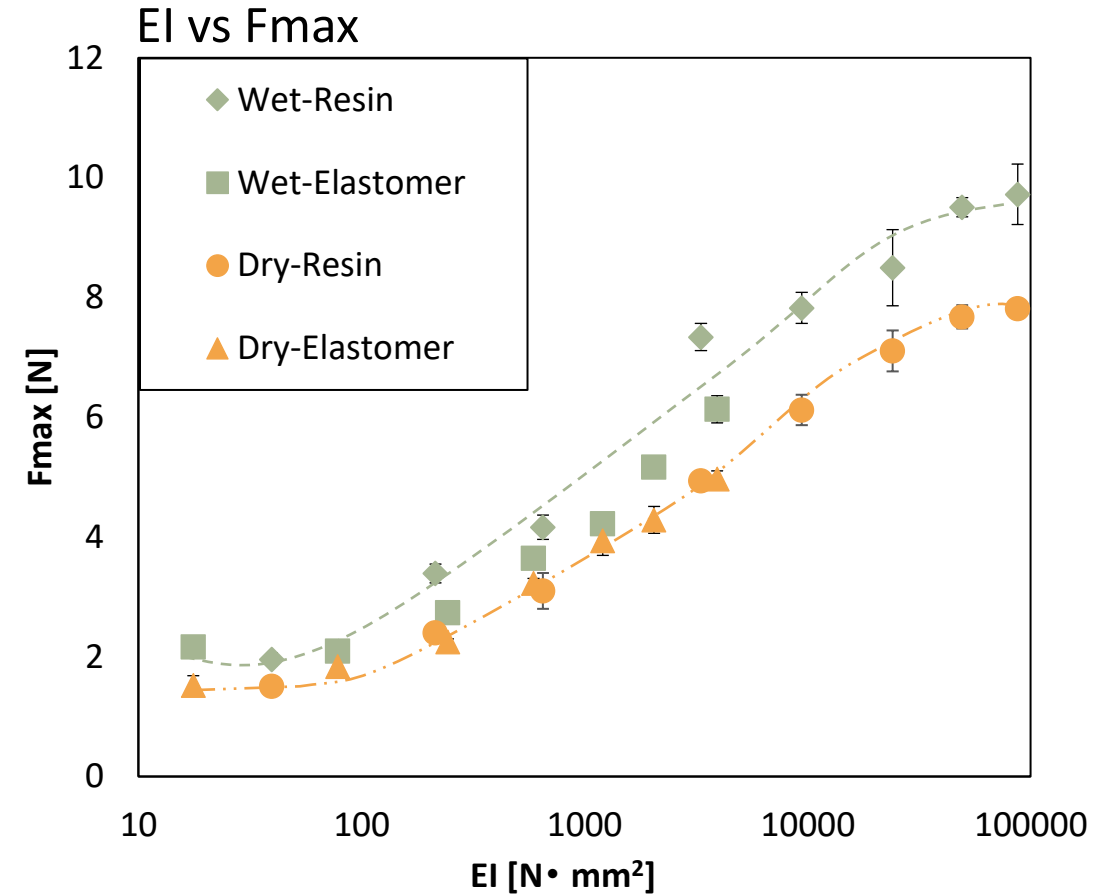
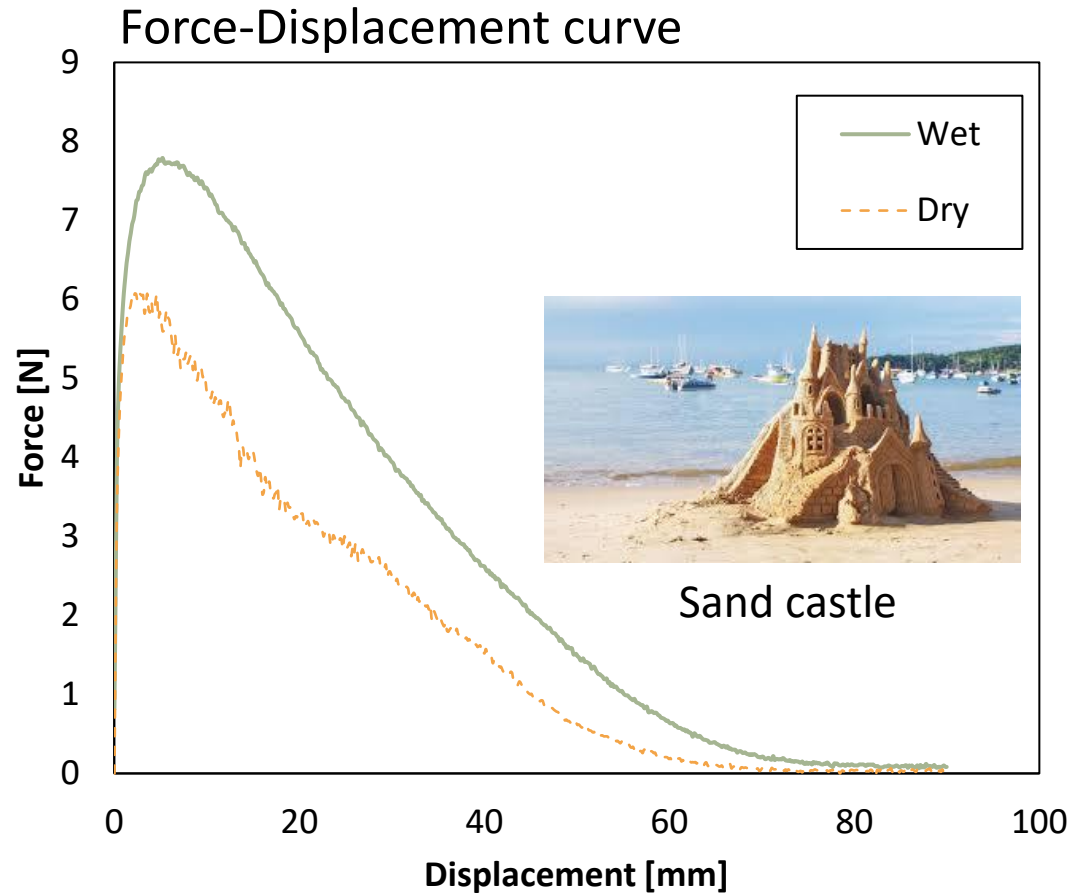
Predicted values for the samples of $D = 2\text{mm}$ (rubber) and $D = 9\text{mm}$ (resin)



Deviation for the $D = 2\text{mm}$ rubber sample is considered to be the resistance for the neck part.

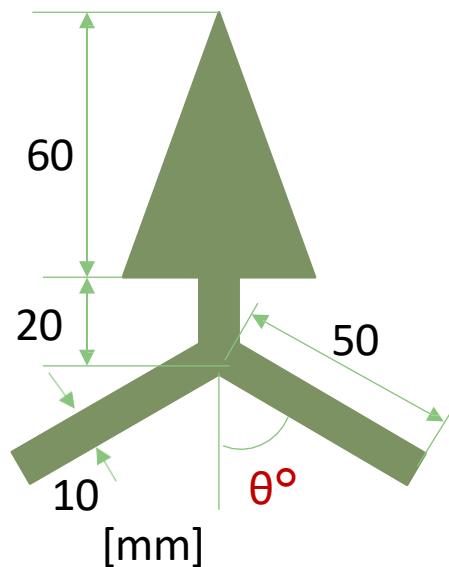
Pullout experiment in wet conditions

Volume fraction of water: 4%



Pushover experiment

- Cedar-like model (T/R ratio $\doteq 3^*$)
Branch Angle $\theta=15, 30, 45, 60, 75, 90$ [°]



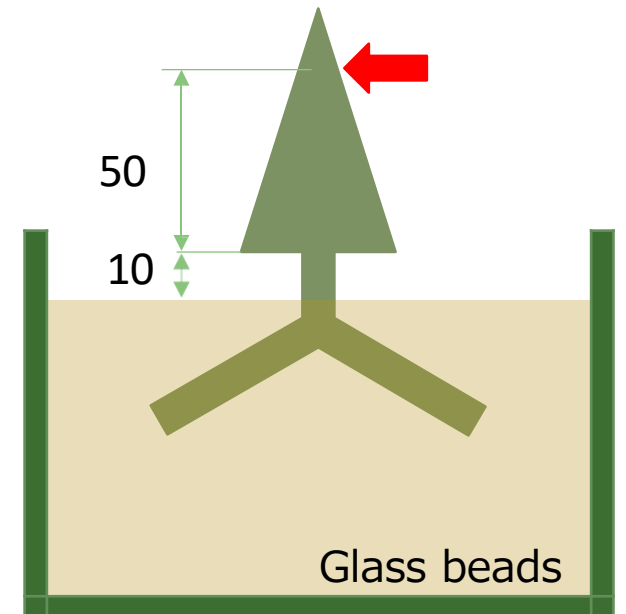
$\theta=30$ [°]



$\theta=60$ [°]

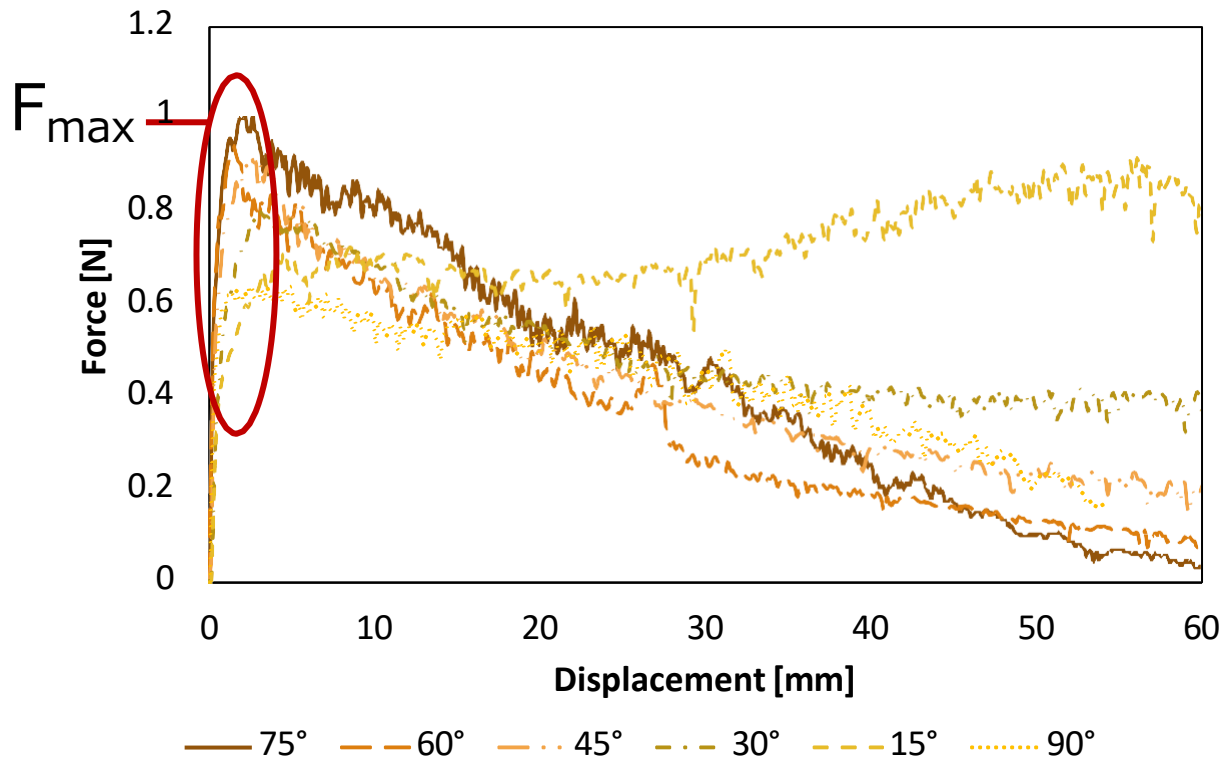


$\theta=90$ [°]



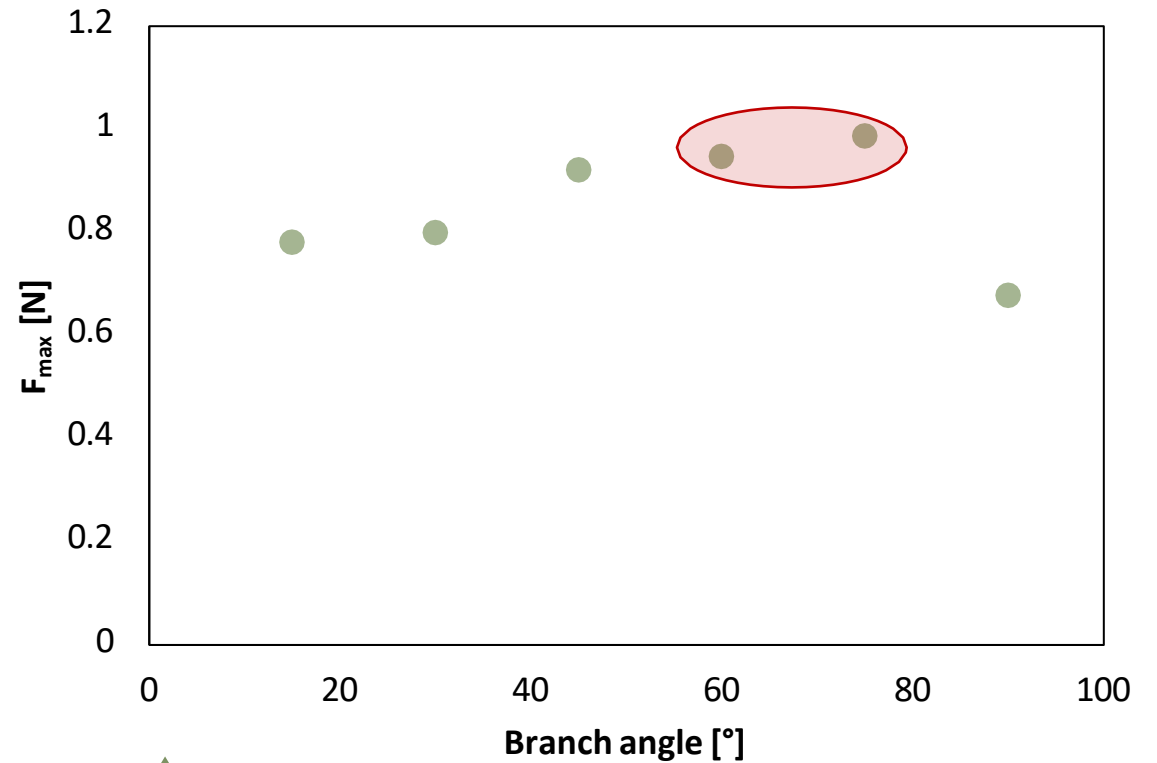
Pushover strength

Force-displacement curve



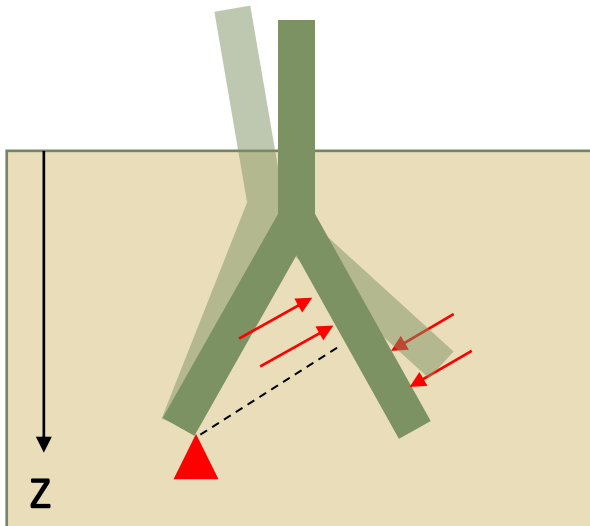
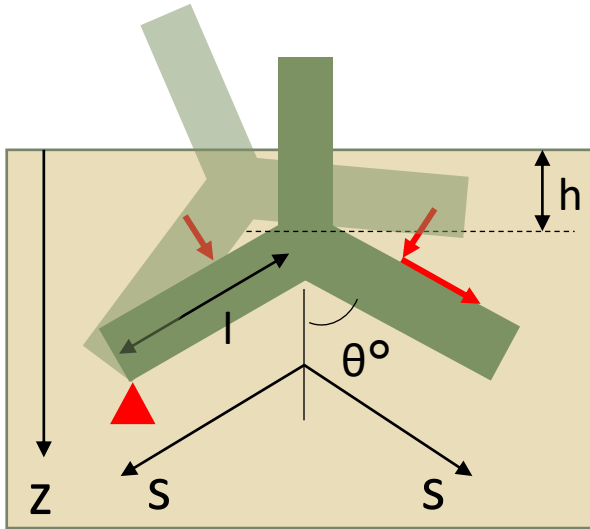
Pushover Force reaches maximum in the early stage

Branch angle - F_{max}



F_{max} reaches a maximum around 60 to 75°

Theory on Pushover



We assume that the stress at fracture is proportional to soil pressure.

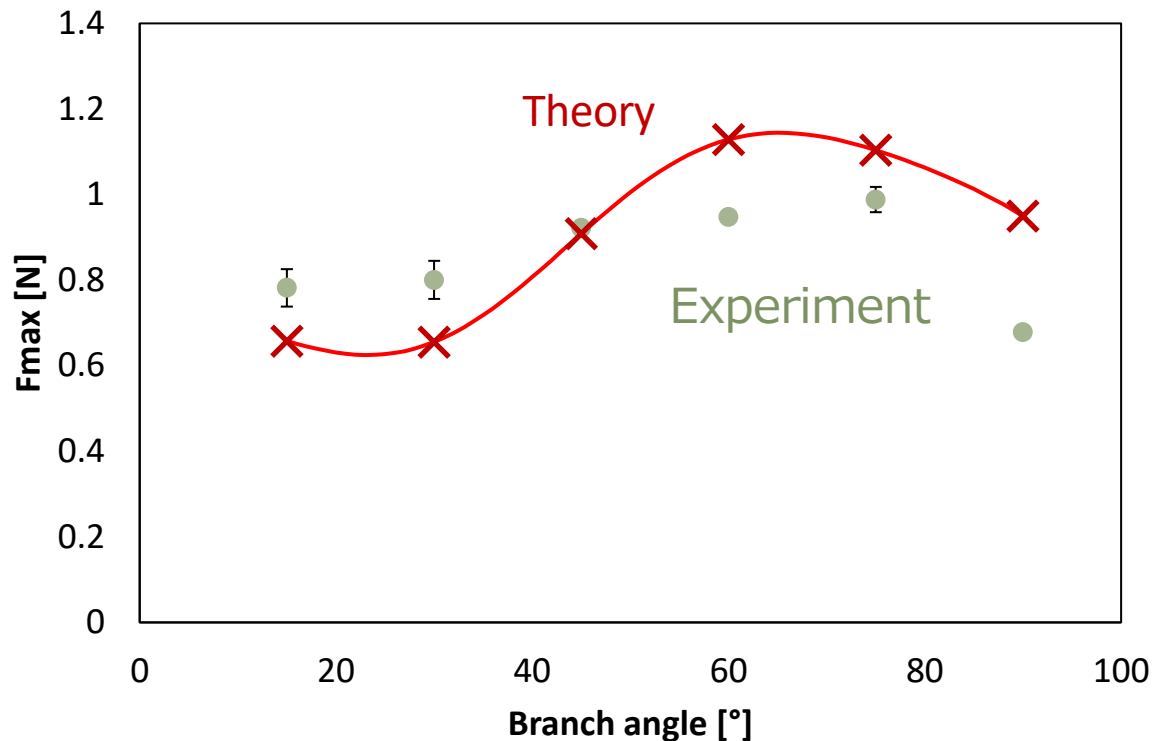
$$\sigma(z) = \sigma_{max} p(z)$$

Total moment

$$M = \frac{\rho g \pi \sigma_{max} D l^2}{2} \left(\frac{8}{3} l \cos \theta^7 - 4l \cos \theta^5 + 4h \cos \theta^4 + l \cos \theta^3 - \right. \\ \left. 6h \cos \theta^2 + \frac{2}{3} l \cos \theta + 3h \right) \\ + \frac{\rho g \pi \sigma_{max} D}{2} h^2 \left(\frac{h}{6} + \frac{l \cos \theta}{2} \right) + \rho g \pi \mu_{max} D \left(hl + \frac{1}{2} l^2 \cos \theta \right) l \sin \theta \cos \theta$$

Calculation result

Branch angle vs F_{\max}



The theoretical curve exhibits an optimum angle $\cong 65^\circ$, in reasonable agreement with experimental results.



The balance between depth and width is important.



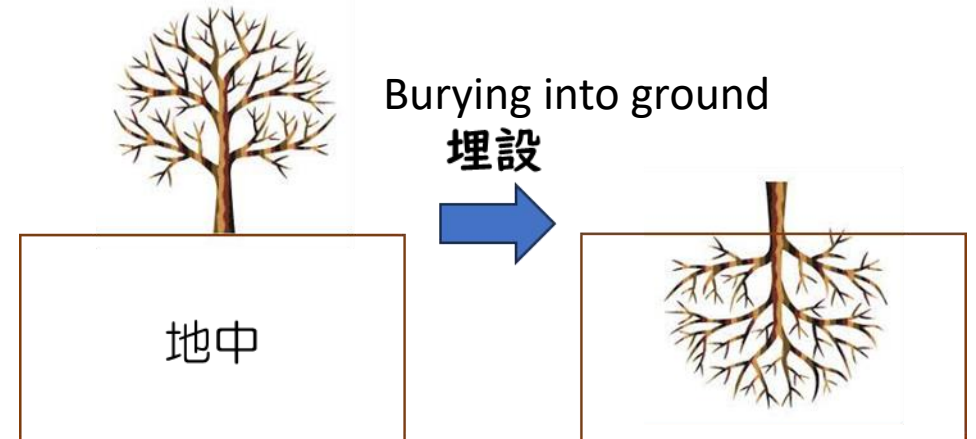
Summary and Future plans

Summary

- We simplified the root structures and conducted pull-out experiments.
- We obtained a strong correlation between bending rigidity and maximum force.
- We successfully described the maximum forces in the flexible and rigid limits.

Future Plans

- Modeling and prediction of mechanical behavior for more realistic root structures and soil
- Engineering application: Soil-reinforcement of slopes using aboveground parts of a tree.



Thank you very much for your attention!

Ex. Rice in budding and growth



Root geometry and soil conditions change with time.

⇒ Is it possible to predict pushover strength during budding and growth?