



イオン 渋滞学
科研費・学術変革(A)



創発的研究支援事業
Fusion Oriented REsearch for disruptive Science and Technology

MOONSHOT
RESEARCH & DEVELOPMENT PROGRAM



Unified understanding of nonlinear rheology near jamming

Nagoya University

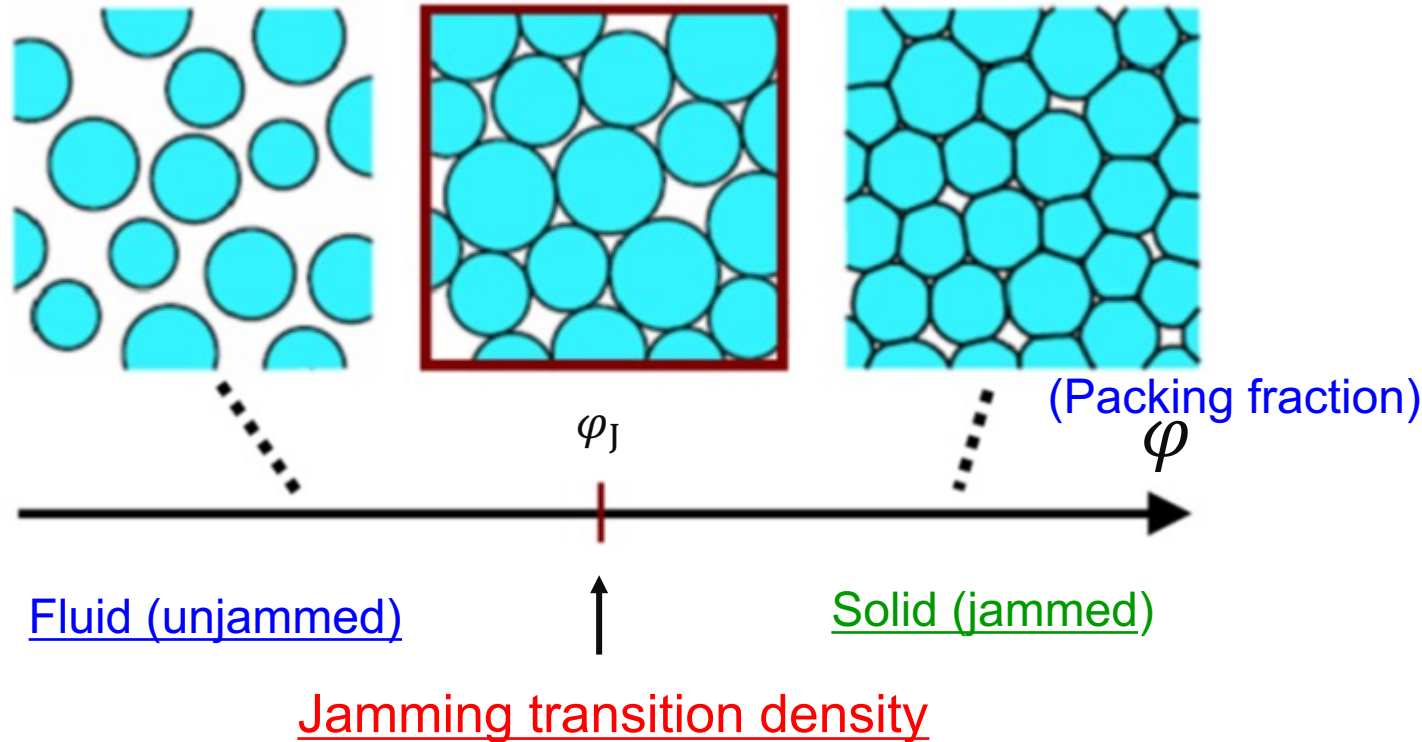
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Collaboration with Kunimasa Miyazaki (Nagoya Univ.)

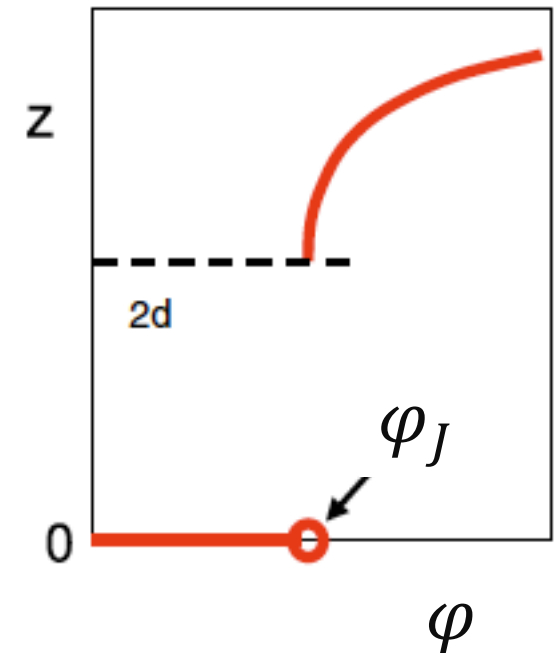
Ref: T. Kawasaki and K. Miyazaki, Phys. Rev. Lett. **132**, 268201 (2024)

Intro: Jamming transition

- Increasing the density of “athermal” particles:
 - ➔ Fluid – solid state transition: **jamming transition**



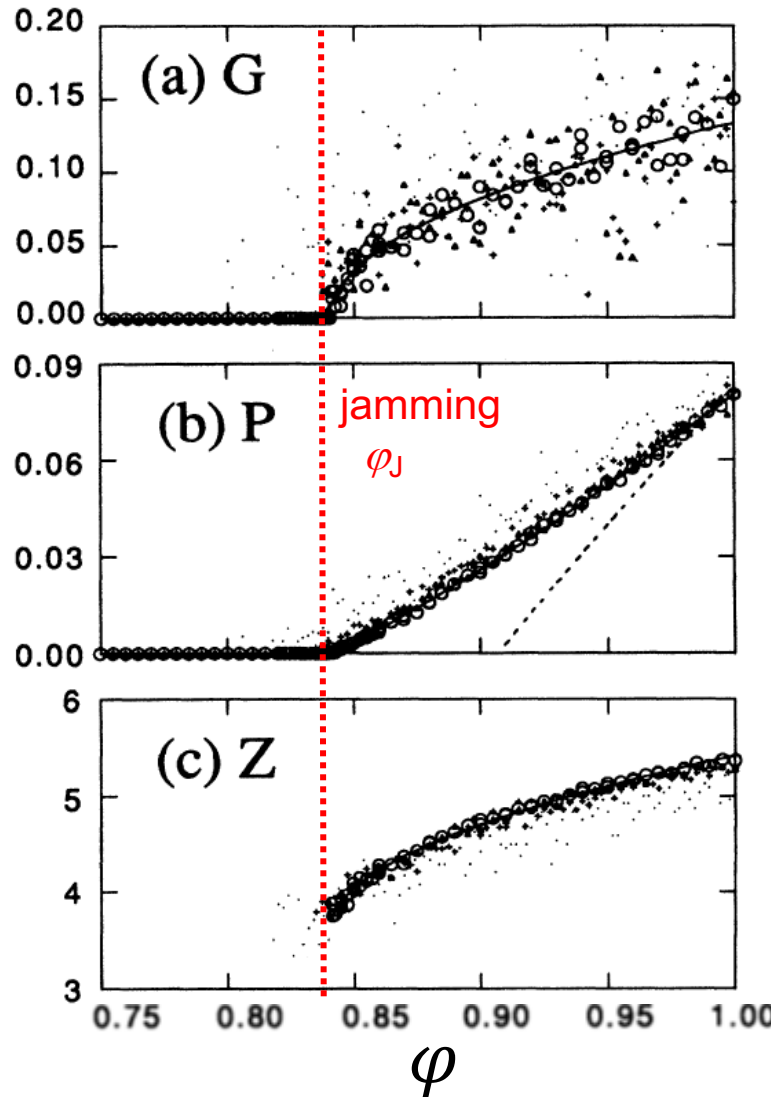
Contact number



- In the vicinity of the jamming transition point ($\varphi = \varphi_J$), mechanical property and mechanical response of the system are critical and nonlinear.

Intro: Critical behaviors near jamming

(a) Shear modulus



(b) Pressure

(c) Contact number

$$G \sim (\varphi - \varphi_J)^{\alpha - \frac{3}{2}}$$

$$P \sim (\varphi - \varphi_J)^{\alpha - 1}$$

α : Hyper-elasticity exponent of the inter-particle potential

$$\Delta Z = Z - 2d \sim (\varphi - \varphi_J)^{\frac{1}{2}}$$

ΔZ : Number of excess contact points

M. Wyart et al., Phys. Rev. E 72, 051306 (2005)

Intro: Typical interaction potential of jammed systems

■ Inter-particle potential (contact force potential)

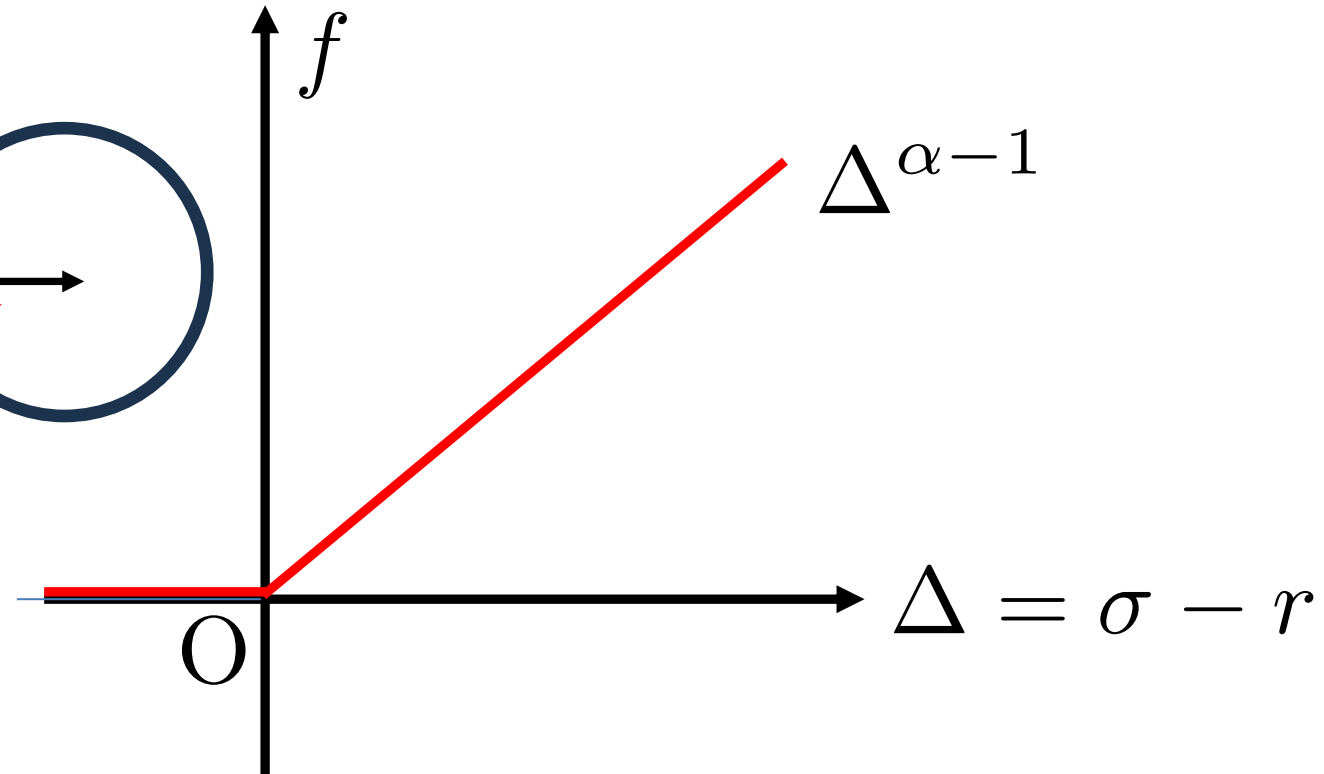
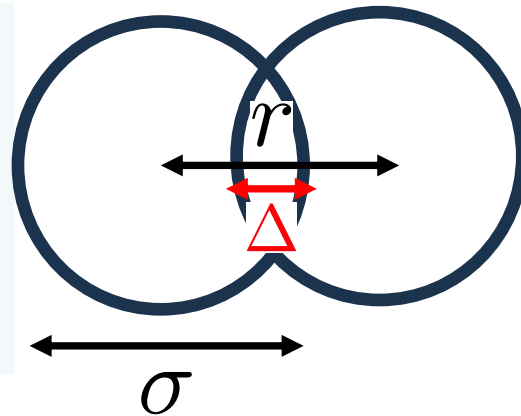
$$U = \sum_{i<j} \epsilon \left(\frac{\sigma_{ij} - r_{ij}}{\sigma_{ij}} \right)^\alpha = \sum_{i<j} k \Delta_{ij}^\alpha$$

$\sigma_{ij} = (\sigma_i + \sigma_j)/2$
 Δ_{ij} : overlap length
 r_{ij} : interparticle distance

■ Supported by Hertzian contact theory

$$\alpha = \frac{5}{2} \quad (3d)$$

$$\alpha = 2 \quad (2d)$$



L.D.Landau and E.M.Lifshitz: Theory of Elasticity (1959)

Intro: Criticality of mechanical properties

- Minute changes in packing fraction from φ_J :

$$\varphi \rightarrow \varphi_J + \delta\varphi$$

φ : packing fraction of particles

$$\sigma_i \rightarrow \sigma_{Ji} + \delta\sigma_i$$

σ_i : diameter of particle i

$$\varphi = \varphi_J + \delta\varphi = \frac{\pi}{6V} \sum_i (\sigma_{Ji} + \delta\sigma_i)^3 \sim \frac{\pi}{6V} \sum_i \sigma_{Ji}^3 \left(1 + \frac{3\delta\sigma_i}{\sigma_{Ji}} \right)$$

$$\delta\varphi \propto \delta\sigma \propto \Delta \text{ (interparticle overlap length)}$$

- Criticality of mechanical properties

$$U \sim Nz\Delta^\alpha \propto \delta\varphi^\alpha \quad (\delta\varphi = \varphi - \varphi_J)$$

$$P \sim U' \sim Nz\Delta^{\alpha-1} \propto \delta\varphi^{\alpha-1}$$

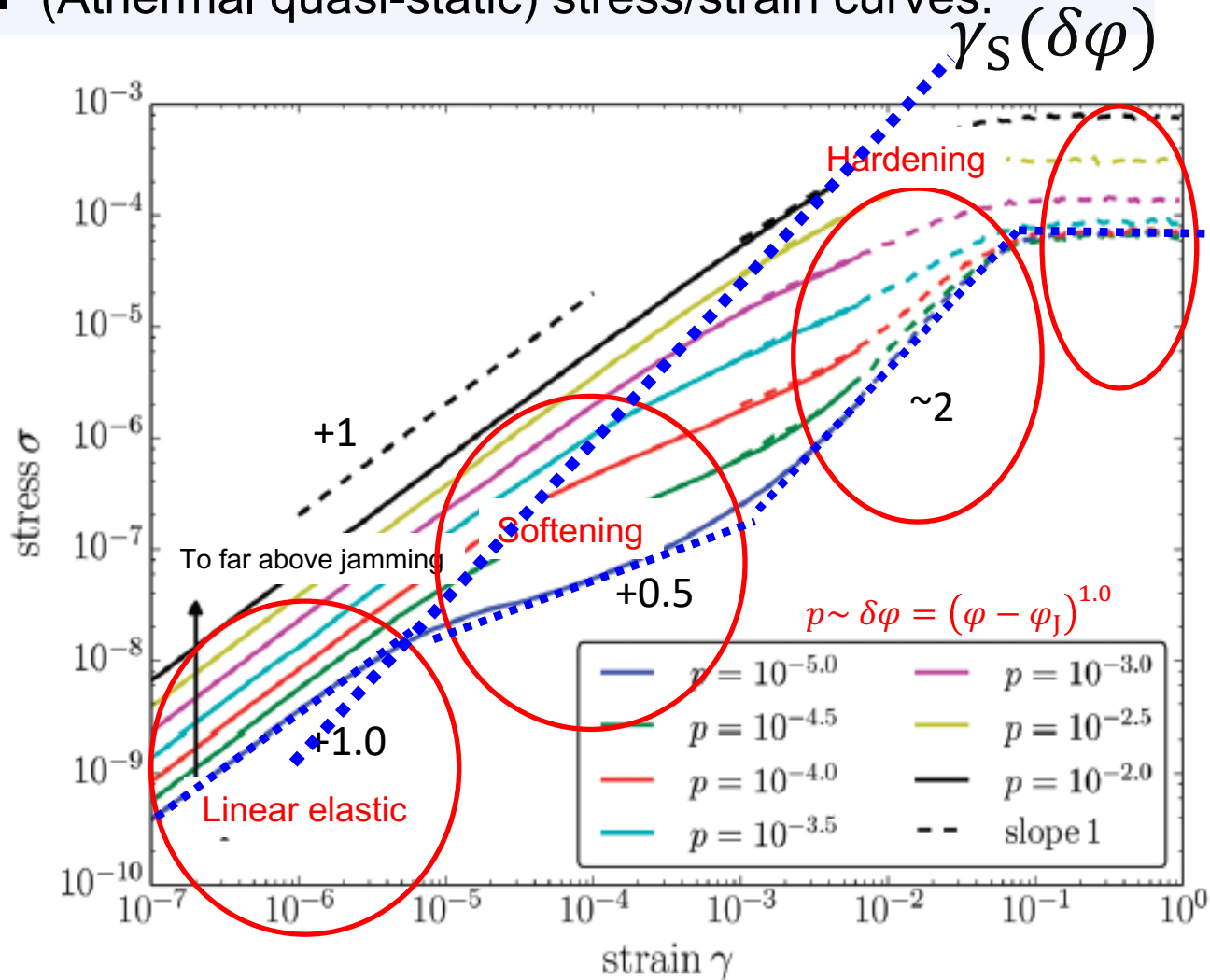
$$B \sim U'' \sim Nz\Delta^{\alpha-2} \propto \delta\varphi^{\alpha-2}$$

➤ all particles sustain the solidity

$$G \sim N\Delta z \Delta^{\alpha-2} \propto \delta\varphi^{\frac{1}{2}} \delta\varphi^{\alpha-2} = \delta\varphi^{\alpha-\frac{3}{2}}$$

Intro: Nonlinear rheology near the jamming transition point

- (Athermal quasi-static) stress/strain curves:



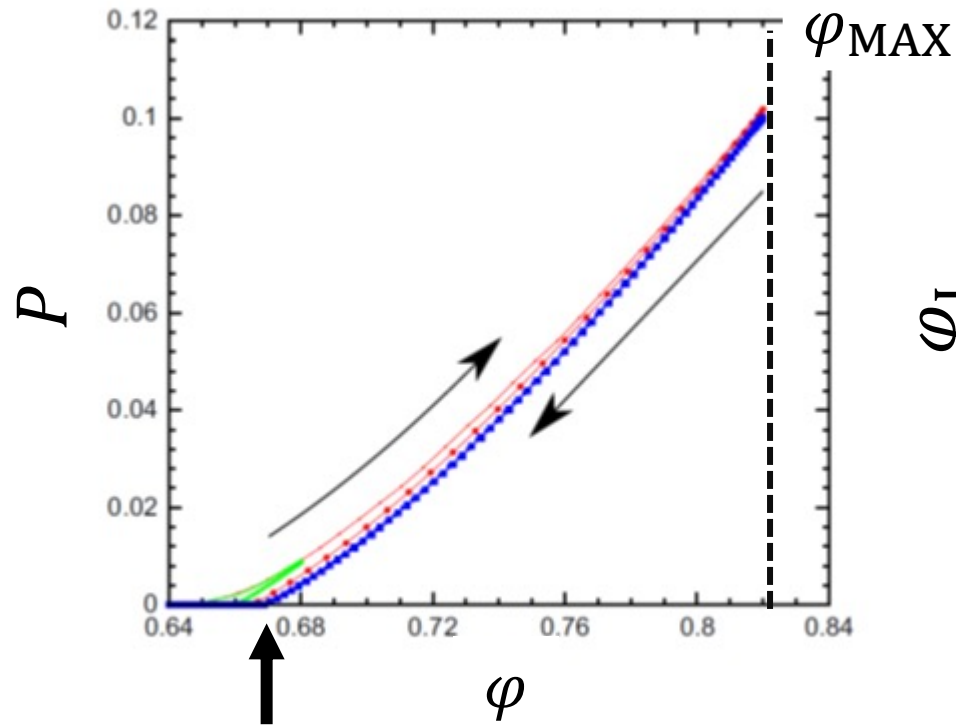
- Becomes extremely complicated near the jamming transition point.
- The curves vary systematically with distance with $\delta\varphi$.
- Critical scaling relations

$$\sigma = \delta\varphi^x \mathcal{F}\left(\frac{\gamma}{\delta\varphi^y}\right),$$
 have been studied intensively but they are still controversial.

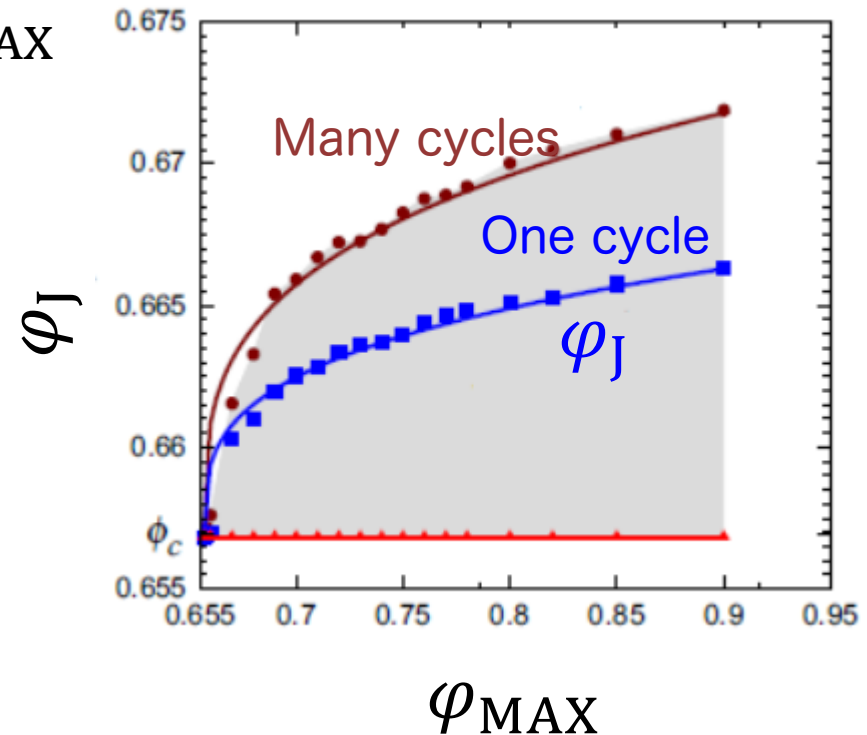
J. Boschan, et al., *Soft Matter* **12**, 5450 (2016).

Intro: φ_J depends on the “history” of the preparations

- Jamming configuration undergoing mechanical training



- φ_J strongly depends on history



φ_J (Jamming transition point for the particle configurations experiencing the training)

N. Kumar and S. Luding, Granular Matter **18**, 58 (2016).

- Scaling of non-linear rheology with respect to $\delta\varphi (= \varphi - \varphi_J)$ needs special attentions, because under large deformation, φ_J should change.

Objectives

- Establishment of jamming critical scaling under large deformations.

Finding:

- Nonlinear rheology contains a protocol-dependent and a protocol-independent part.
- By their disentanglement, we establish a precise critical scaling law.

T. Kawasaki and K. Miyazaki, Phys. Rev. Lett. **132**, 268201 (2024)

Methods

■ Athermal quasi-static (AQS) simulation:

- FIRE method [E. Bitzek, et al., Phys. Rev. Lett. 97, 170201 (2006)]: minimize energy at each step.
- Mainly two-dimensional systems (equivalent for three-dimensional systems)

■ Interaction potential:

- Mainly harmonic potential:

$$U = \sum_{i < j} \frac{\epsilon}{2} \left(1 - \frac{r_{ij}}{\sigma_{ij}} \right)^2 .$$

■ Particle size dispersion:

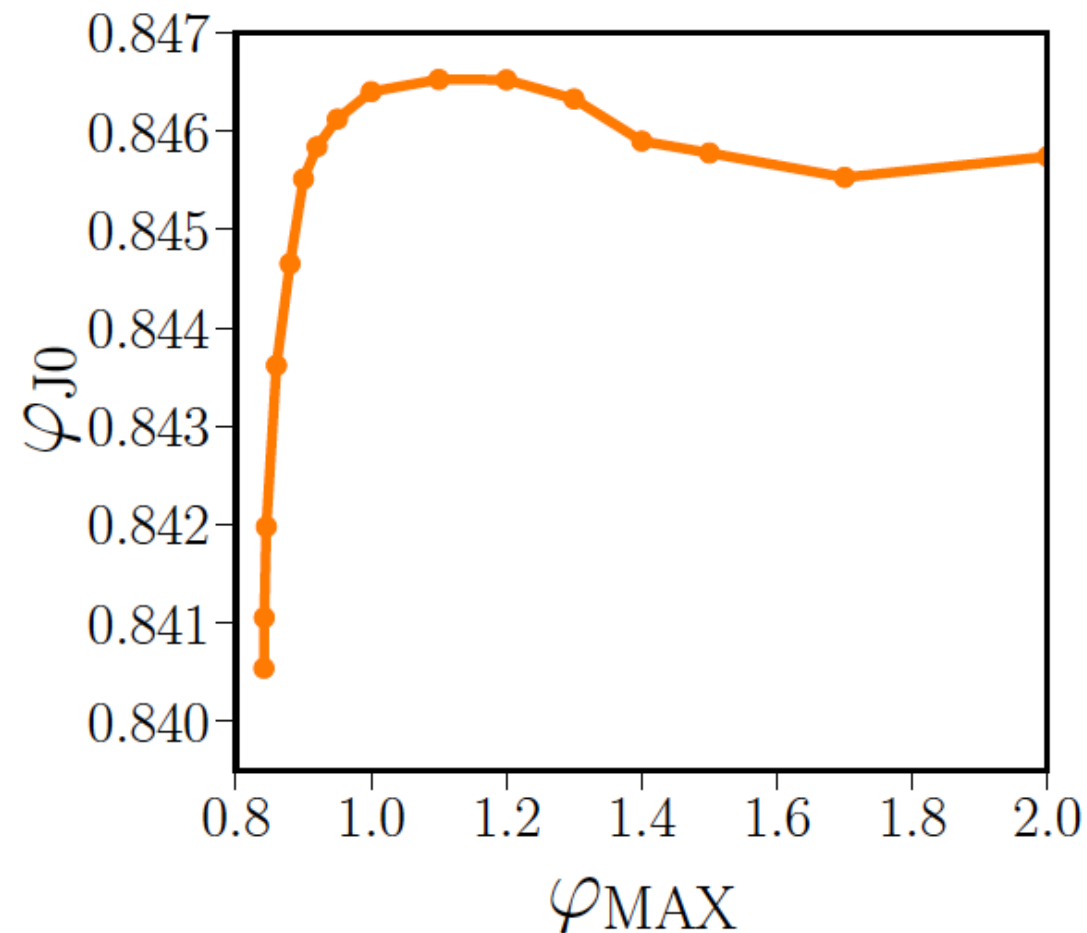
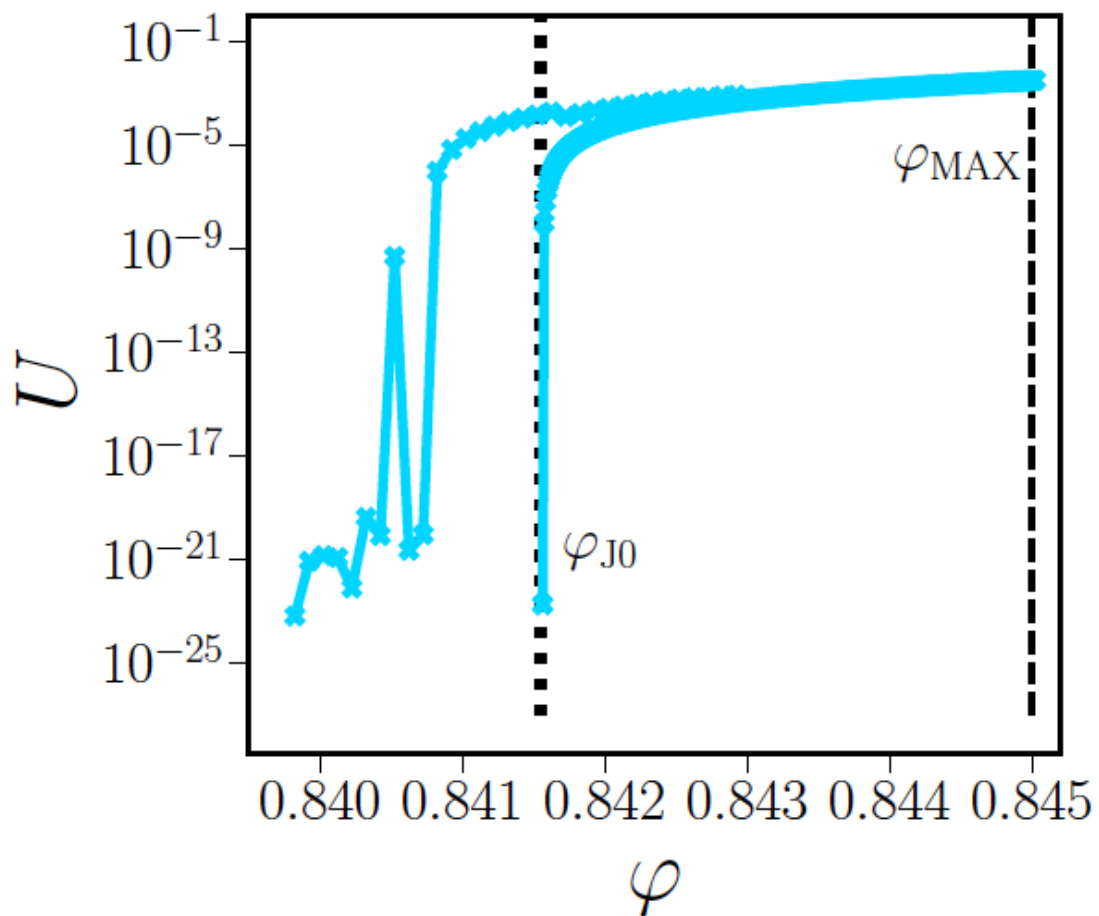
- Binary mixtures (size ratio 1.0:1.4, particle number ratio 1:1)

■ Frictionless particles

Result: Generation of jamming configuration

■ For the test of protocol dependence:

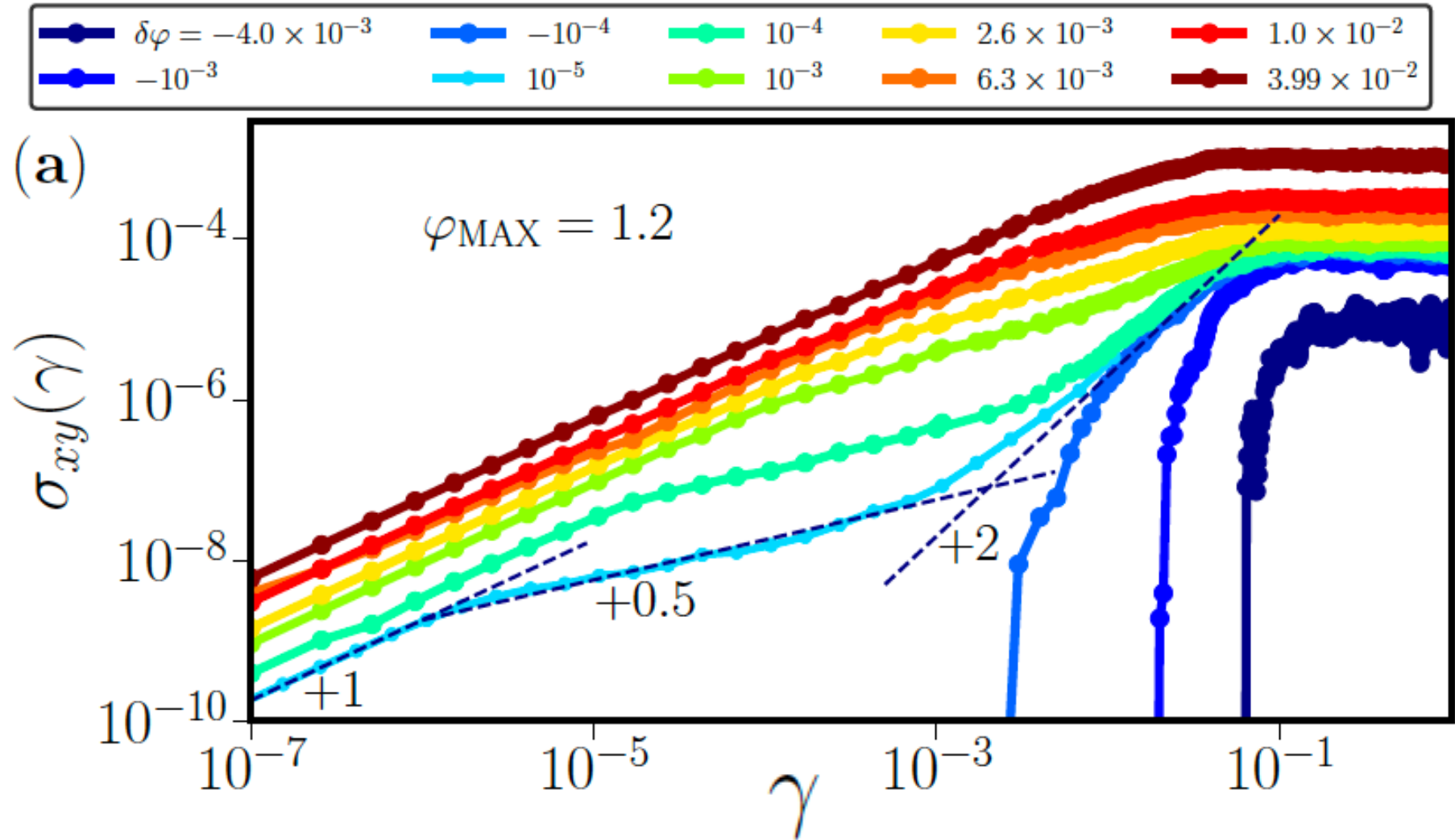
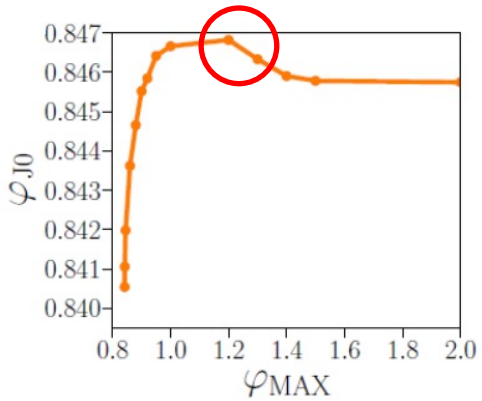
- Generate **varieties** of initial conditions by the systematic mechanical training.



- Changing the density of **each jamming configuration**.
- Applying AQS shear flow.

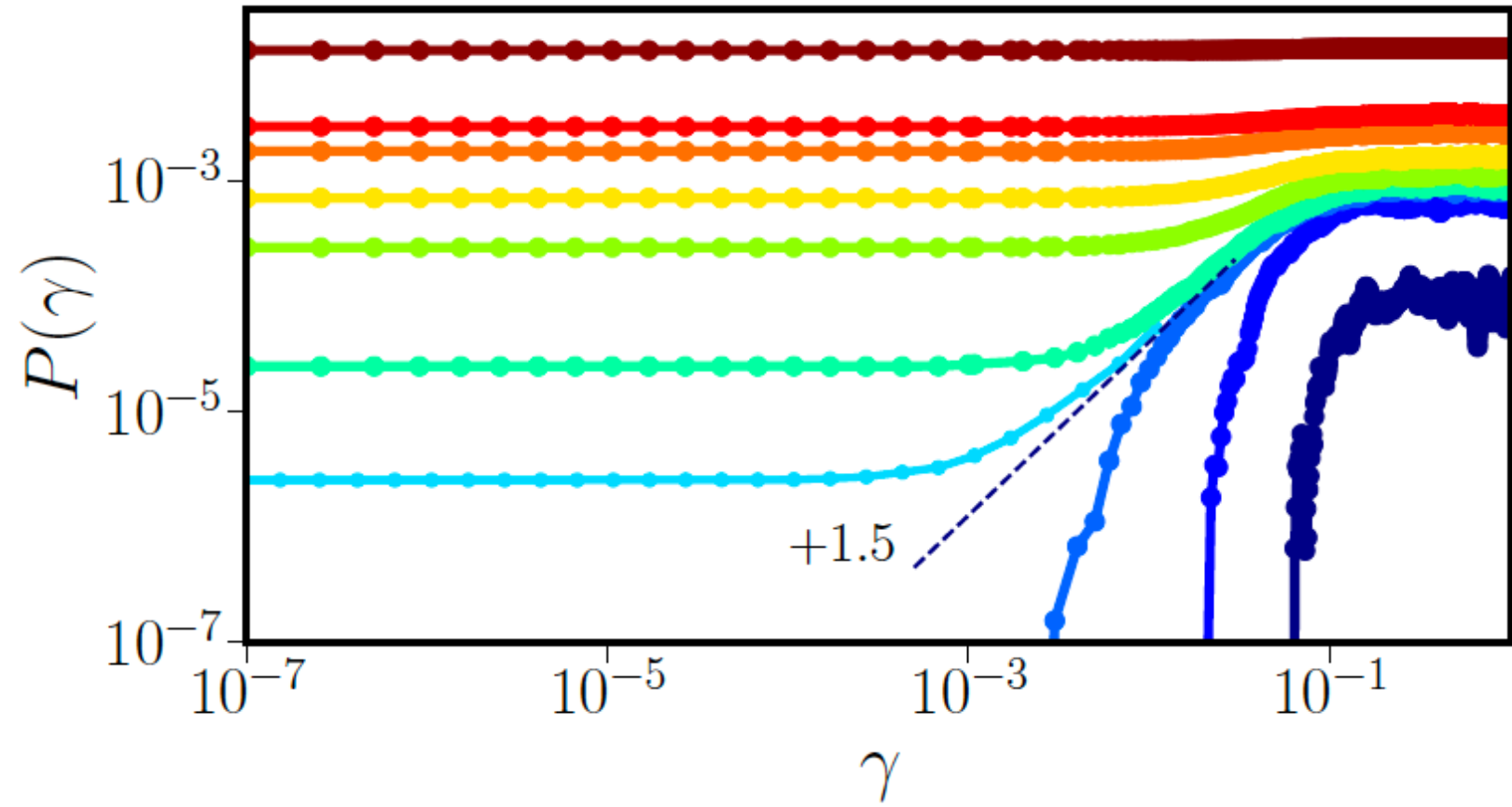
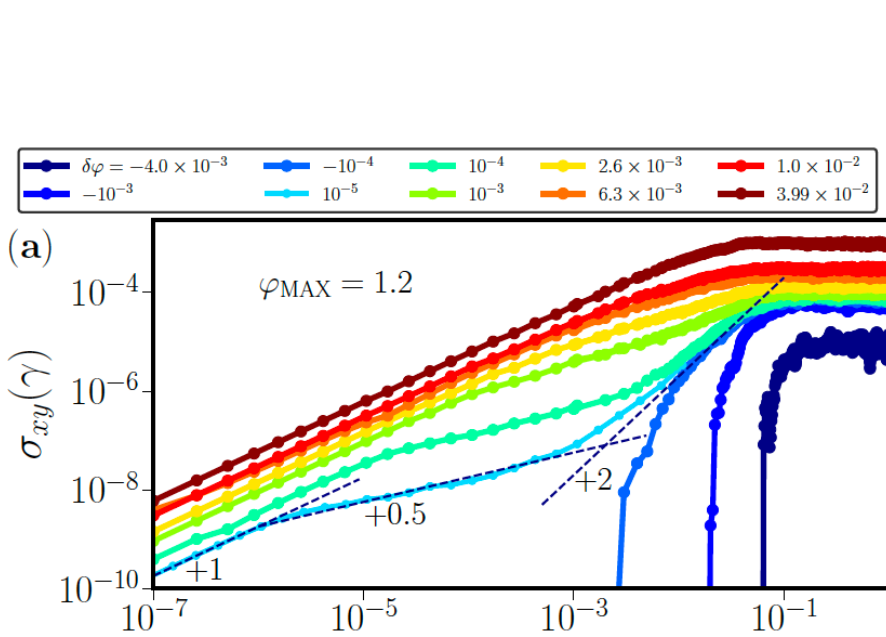
Result: Stress-strain curve under constant volume

- φ -dependence of stress/strain curves under constant volume (at well-trained system $\varphi_{\text{MAX}} = 1.2$)



➤ Elastic, softening, hardening, shear jamming, and yielding are observed.

Result : Pressure-strain curve **under constant volume** ($\varphi_{\text{MAX}} = 1.2$)



$$P(\gamma) \sim (\varphi - \varphi_J(\gamma))$$

Pressure change = Change in jamming point

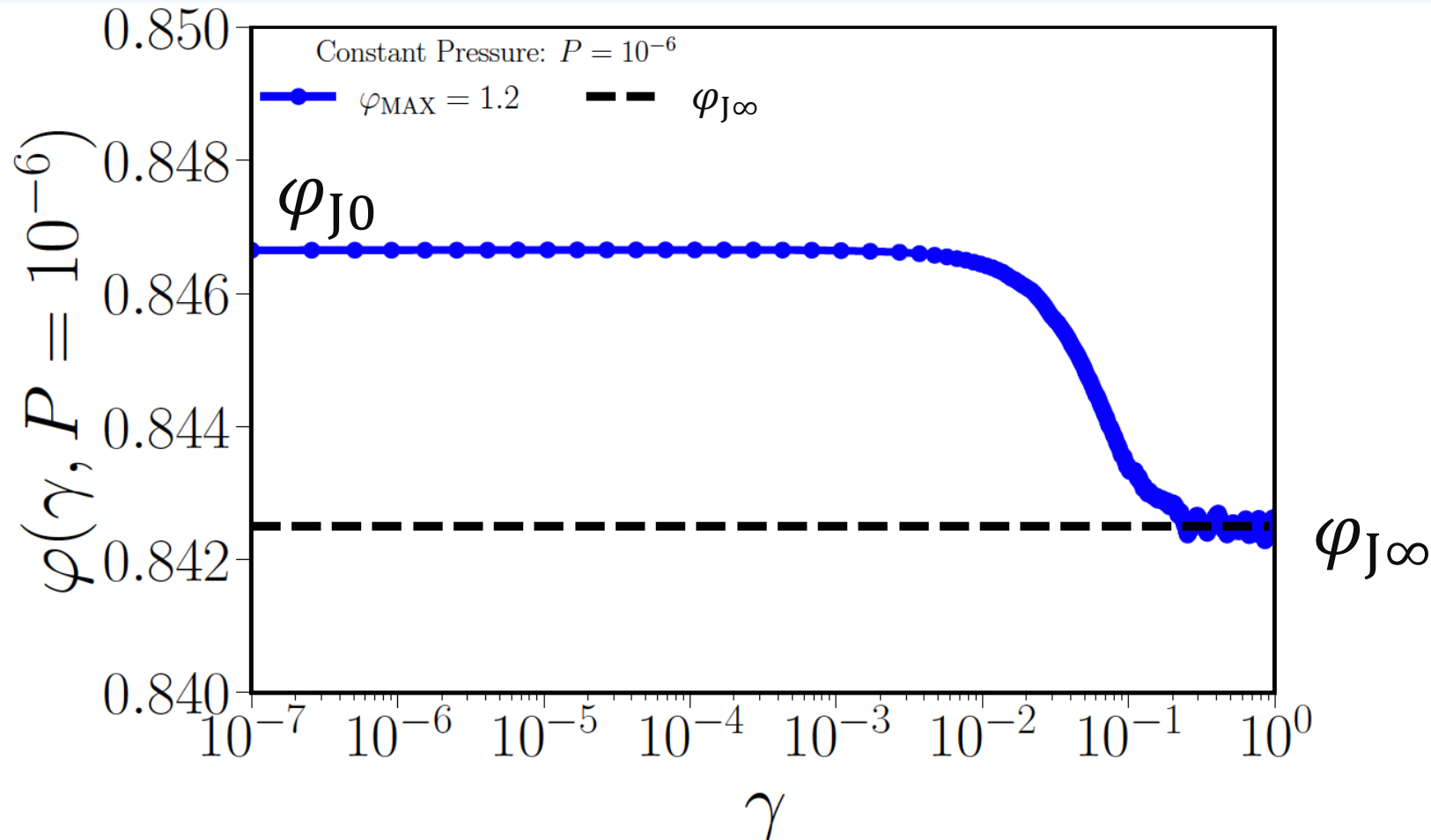
Result: Change in jamming point while shearing

- Computing φ_J under shear deformation:

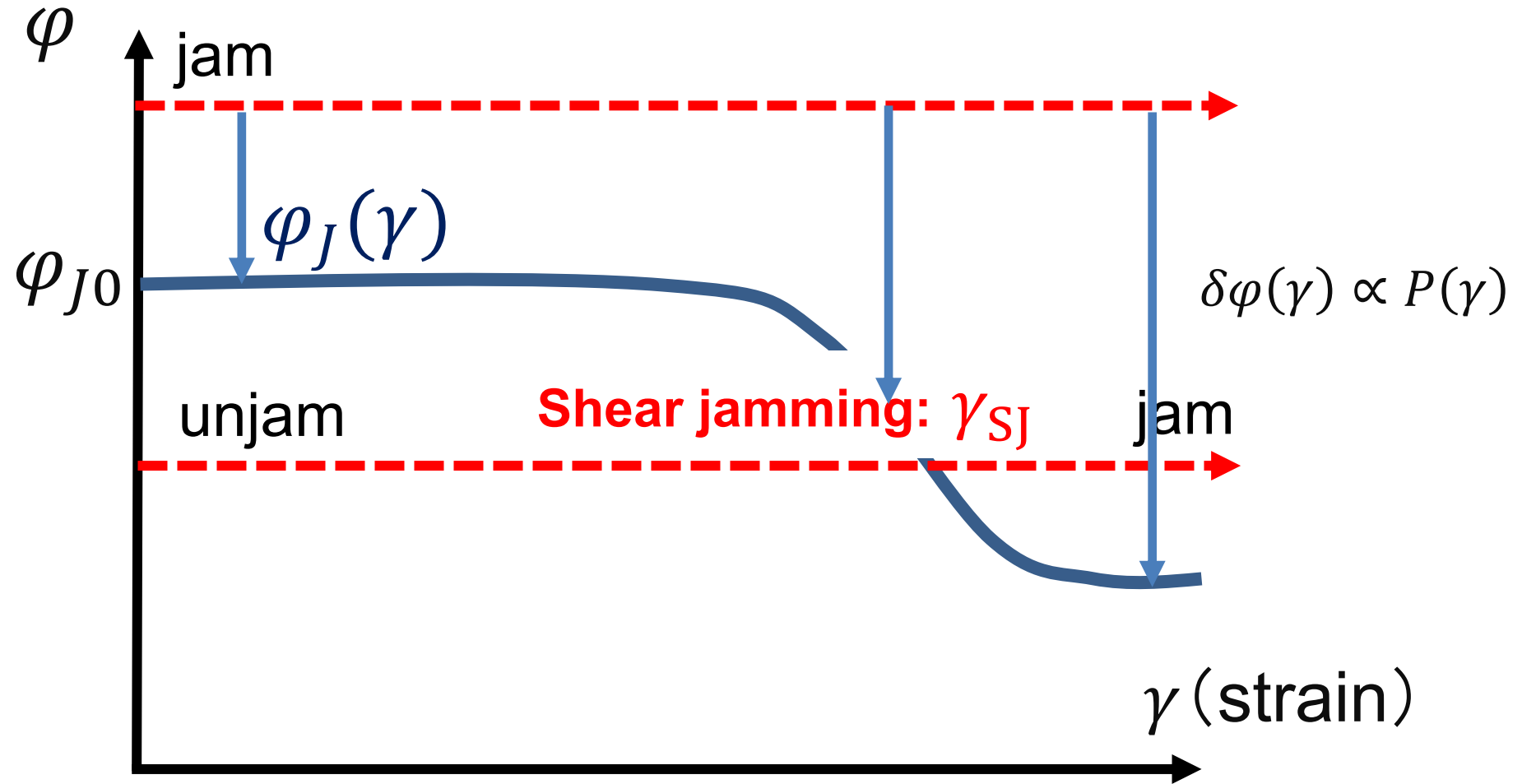
- Fixing at a very small pressure and tracking density

$$P(\gamma) \propto \delta\varphi(\gamma) = \varphi(\gamma) - \varphi_J(\gamma) \ll 1$$

$$\therefore \varphi(\gamma) \sim \varphi_J(\gamma)$$

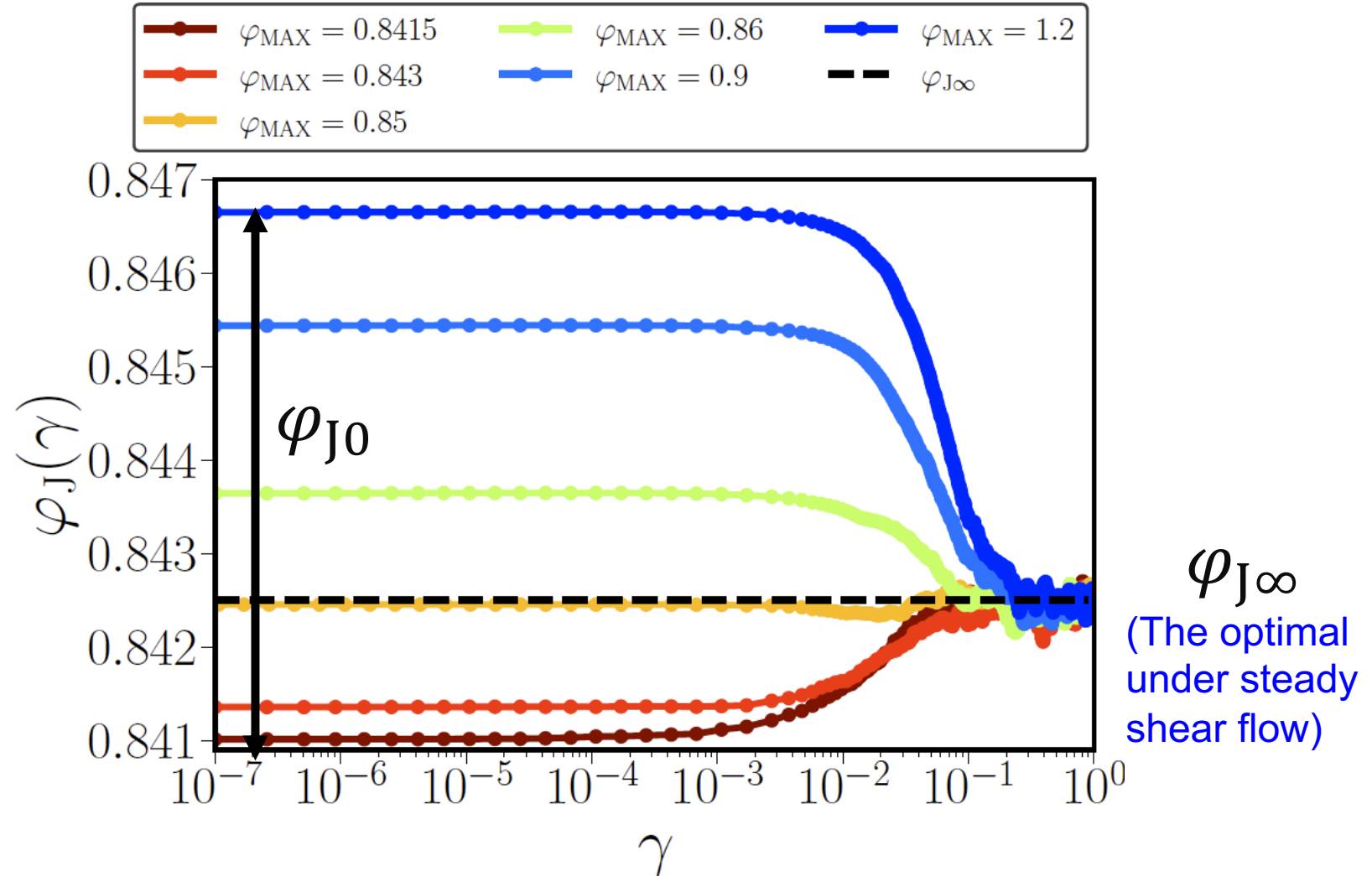
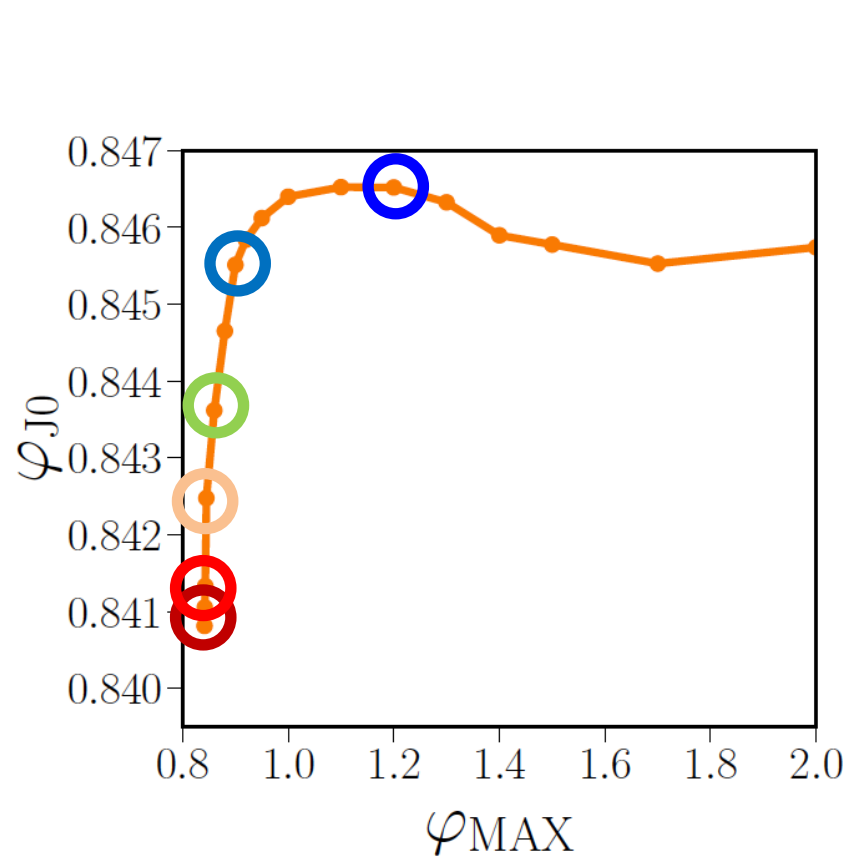


Discussion: Origin of shear hardening and shear jamming



Result: Change of the jamming transition density by steady shear

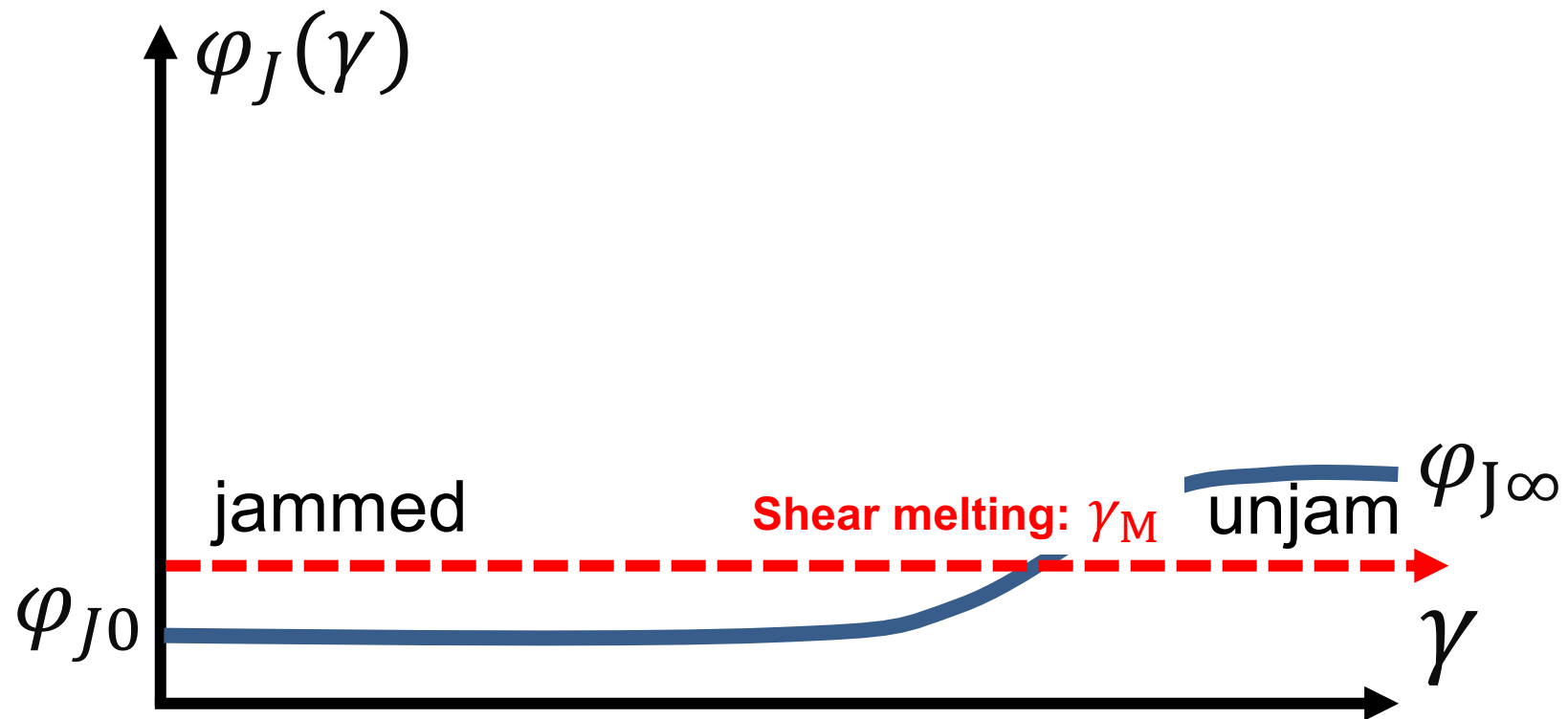
- Estimating the $\varphi_J(\gamma)$, for various annealing intensities φ_{MAX} .



➤ ill-trained configurations: φ_J increases by applying γ .

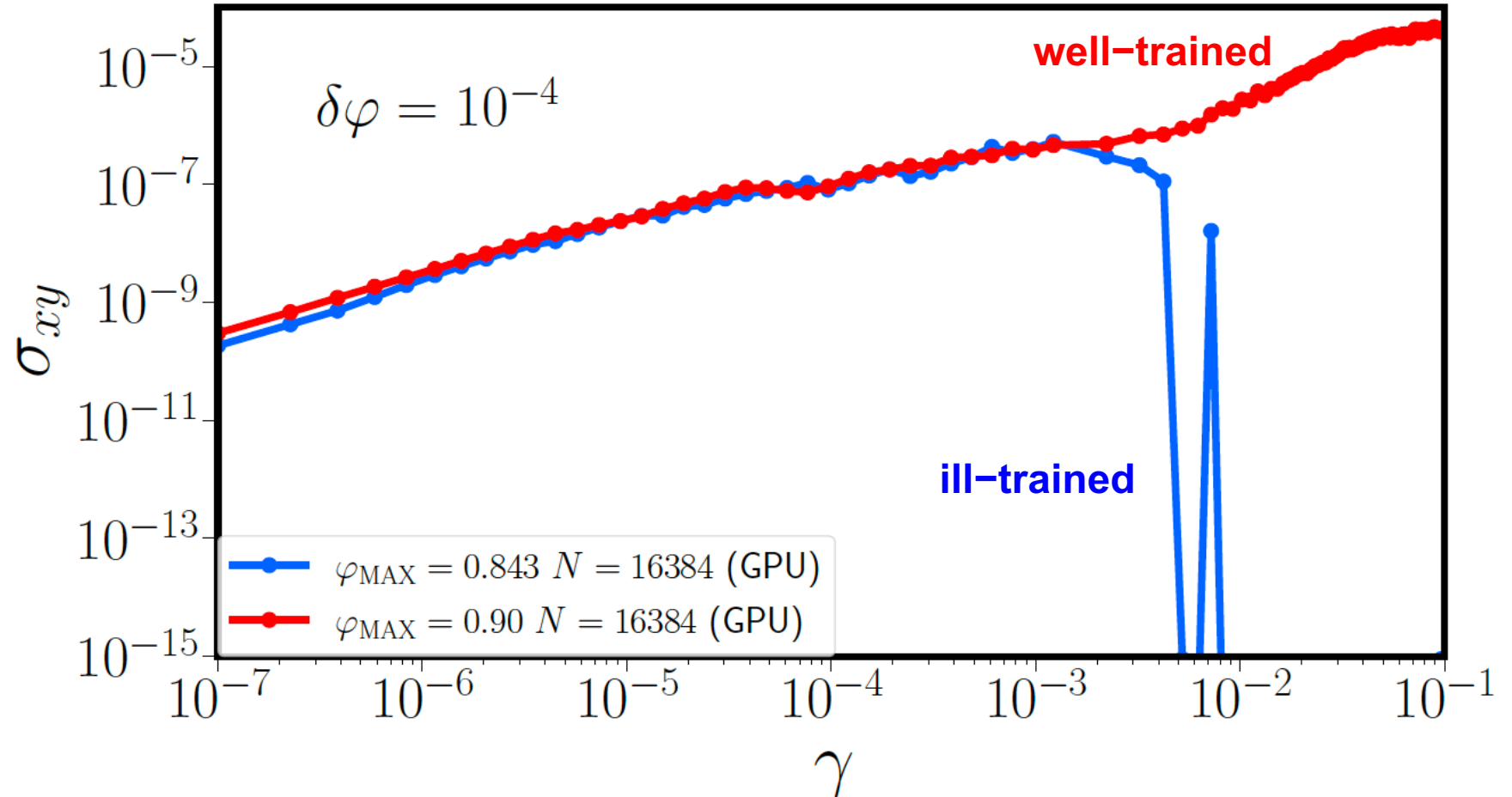
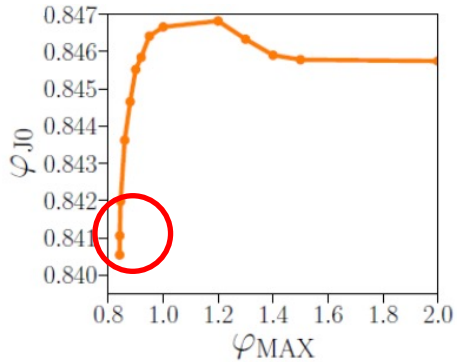
Discussion: Shear melting

- An ill-trained case: **shear melting takes place.**



The mechanical responses of an ill-trained system

- **Constant volume** stress-strain curves near jamming at $\varphi_{\text{MAX}} = 0.843$ (**ill-trained system**).

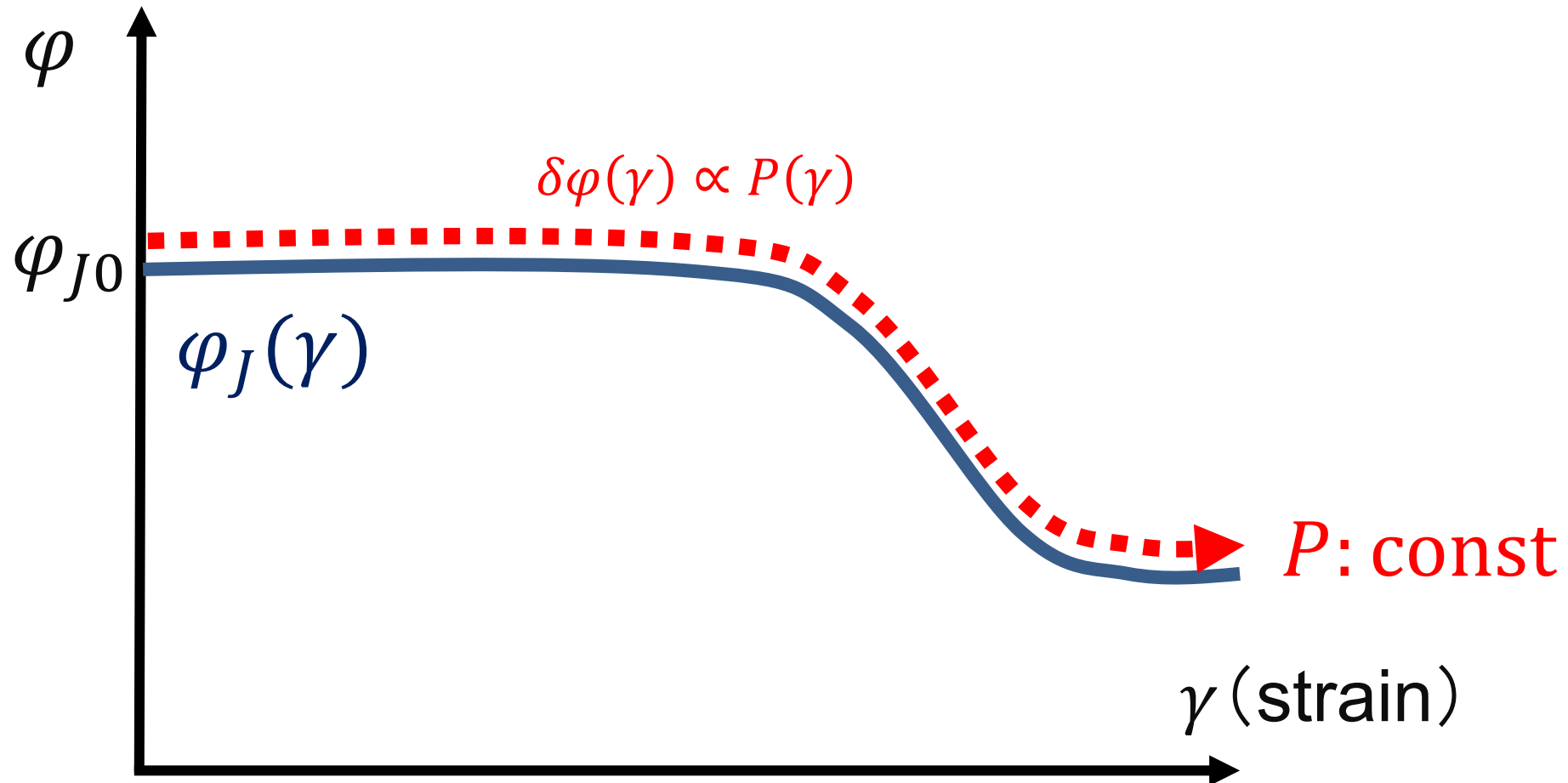


- The system melts under shear flow -- shear melting takes place.

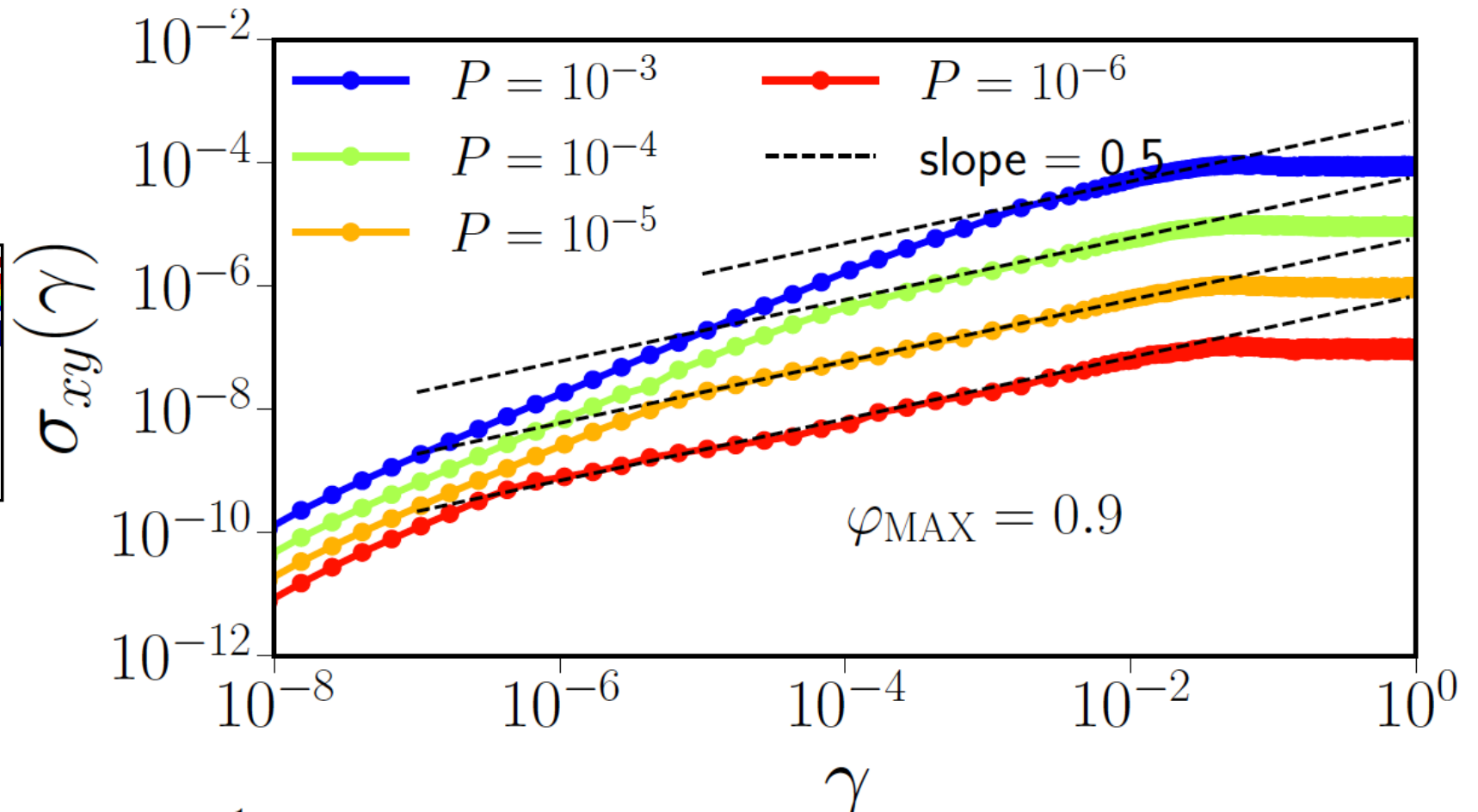
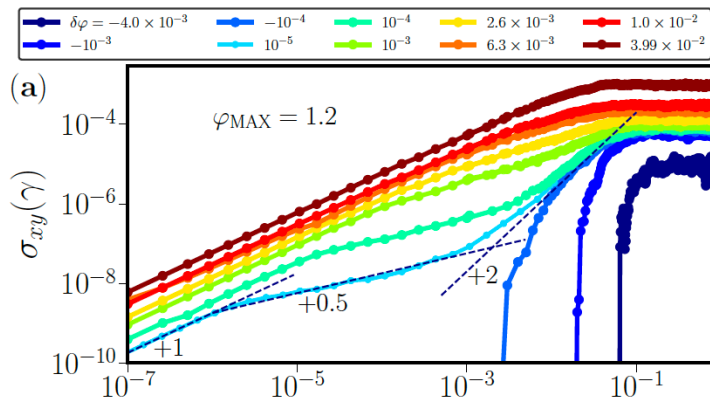
Discussion: Constant pressure makes $\delta\varphi$ keep constant

- The change in $\delta\varphi$ at constant volume is protocol-dependent, and inconvenient for critical scaling.

➤ Constant pressure makes $\delta\varphi$ keep constant.

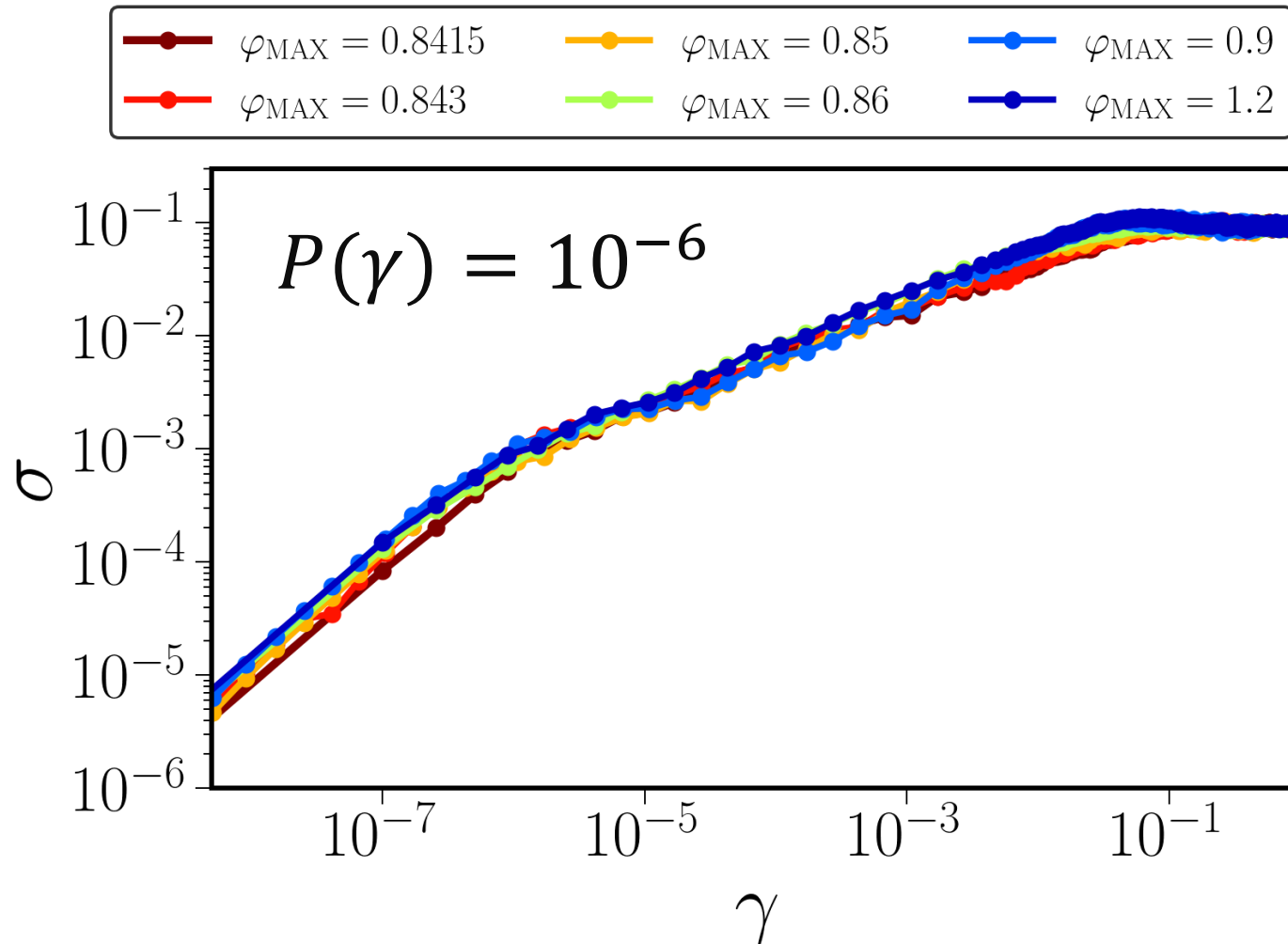
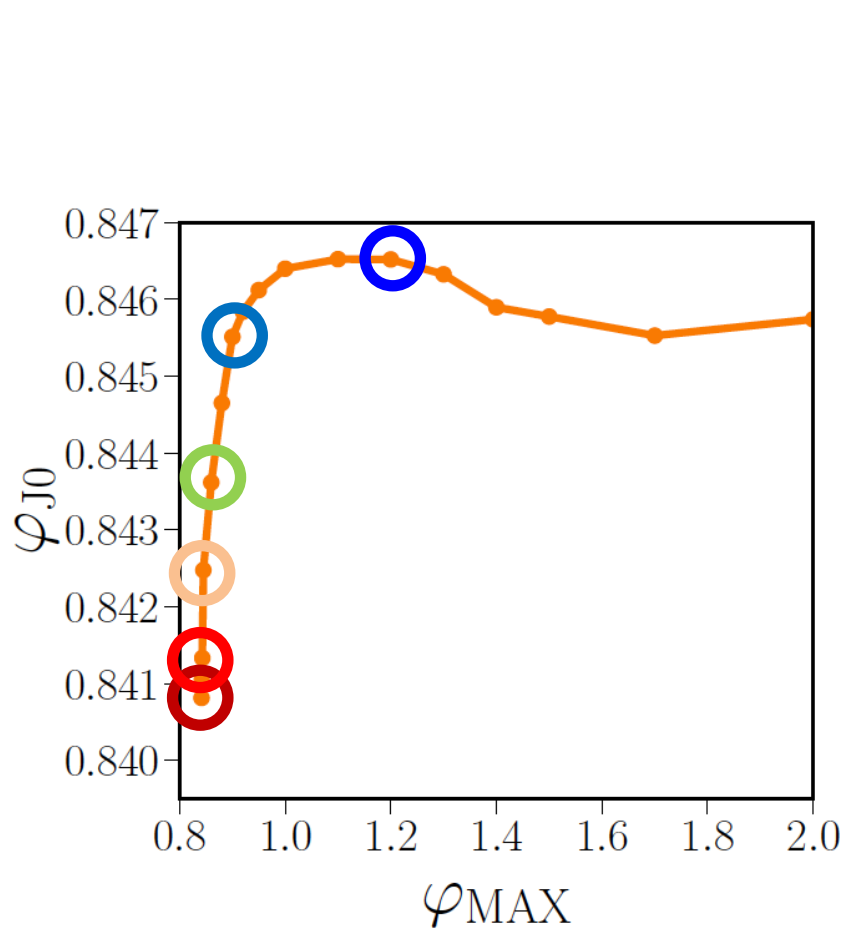


Result: Stress-strain curves under constant pressure



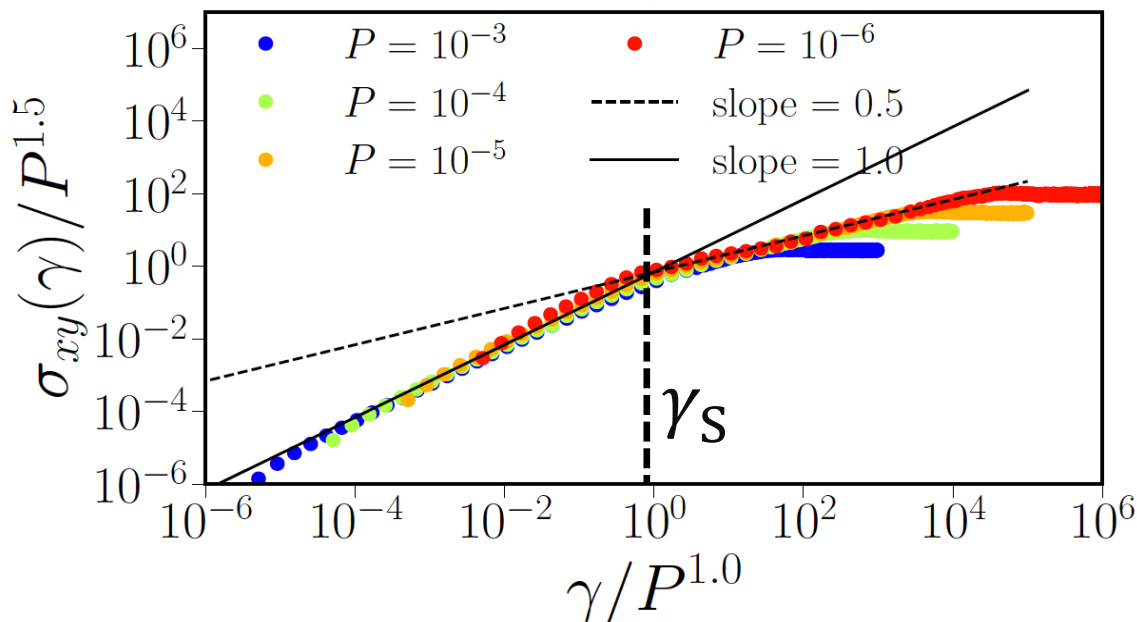
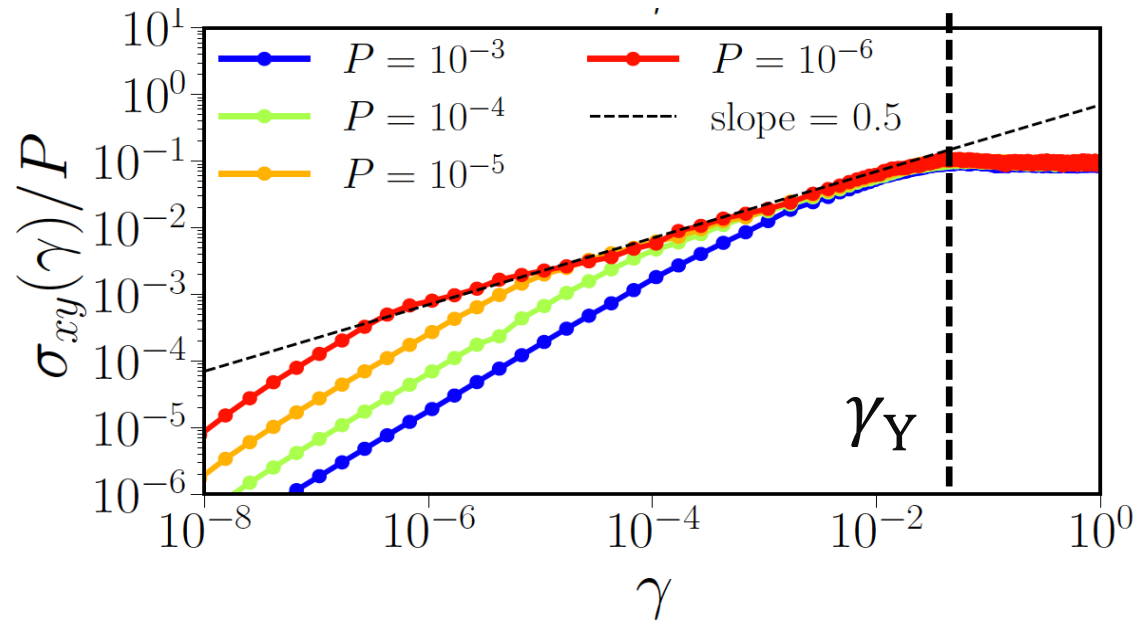
- A hardening disappears.
- Finding the connection between softening and yielding.

Result: The protocol dependence on the non-linear rheology



- We get protocol independent mechanical response!
- Expect reliable scaling relationships.

Result: Scaling relations (at constant pressure)



Yielding:

- $\sigma_{xy}(\gamma \rightarrow \infty) \sim P_{\gamma \rightarrow \infty} \sim \varphi - \varphi_{J\infty}$

Softening onset:

- $\gamma_Y \sim 0.1$

Softening:

- $\sigma(\gamma) \sim (\delta\varphi)^{1.0} \gamma^{0.5} = P(\gamma) \gamma^{0.5}$

Elastic onset:

- $\gamma_S \sim \delta\varphi^{1.0} \sim P$

Cf: M. Otsuki and H. Hayakawa, Phys. Rev. E 90, 042202 (2014)

➤ Explain why such scaling is established from a microscopic view point.

Discussion: Microscopic dynamics and structure (under constant pressure)

(Assume) Softening is attributed to the reconnection of interparticle overlap.

■ Interparticle overlap

$$\langle \Delta r_{\text{overlap}} \rangle \sim \delta\varphi \sim P$$

■ Cage relative (CR) displacement

$$\langle \Delta r_{\text{CR}} \rangle \sim \gamma$$

➤ Softening conditions:

$$\langle \Delta r_{\text{CR}} \rangle > \langle \Delta r_{\text{overlap}} \rangle$$

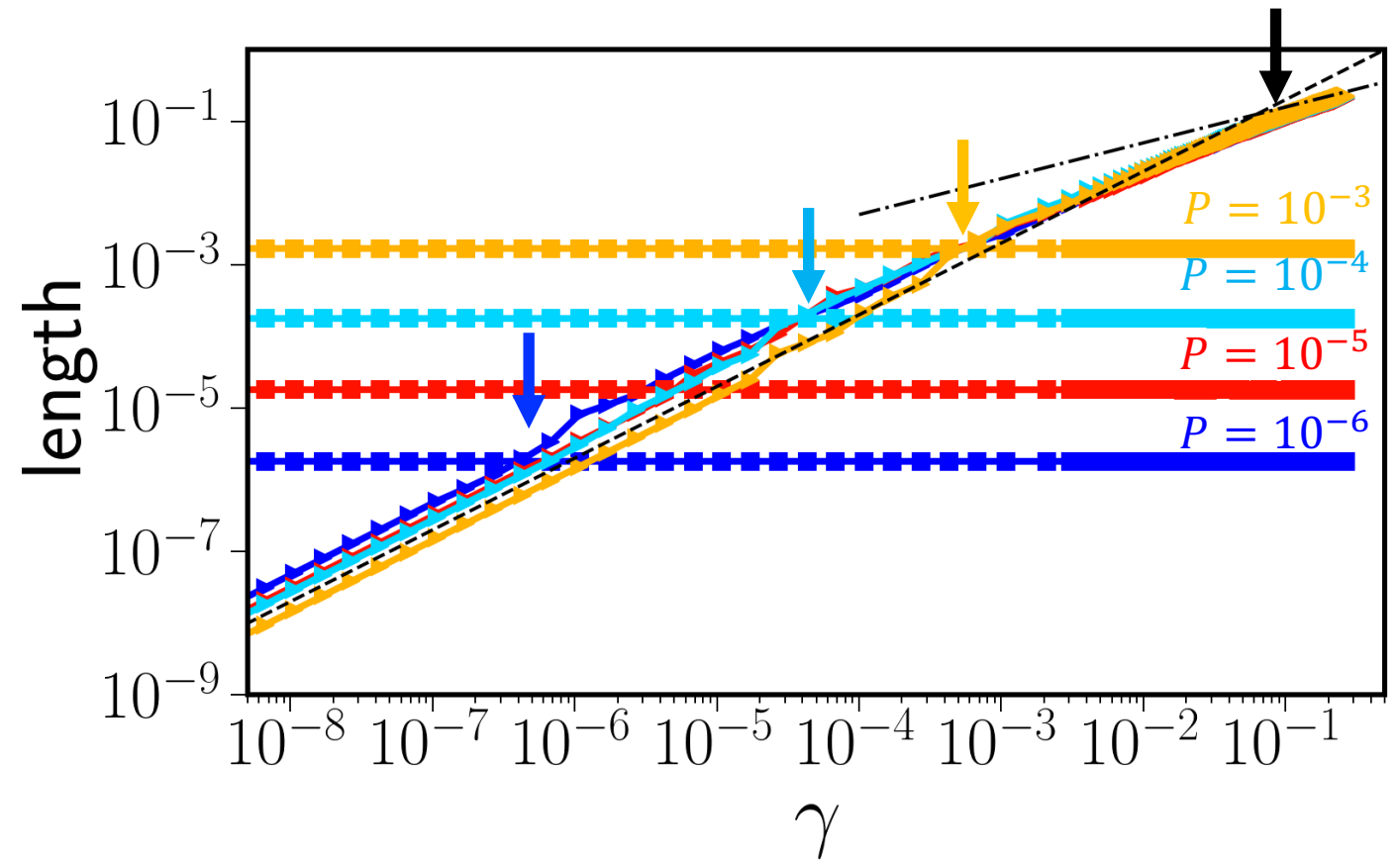
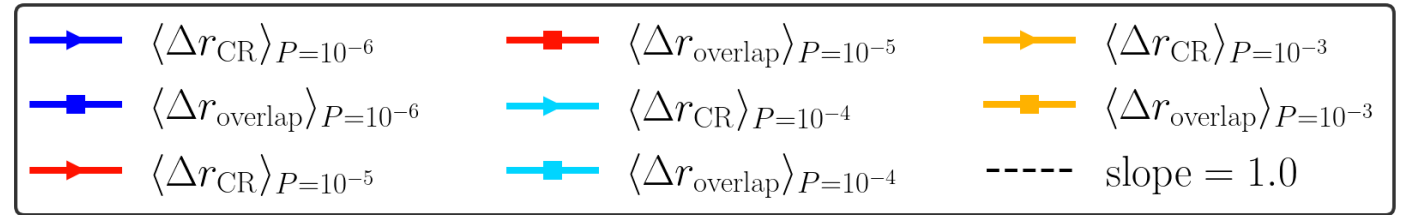
$$\therefore \gamma_S \sim \delta\varphi$$

Yielding occurs when the cages are broken.

■ Yielding condition:

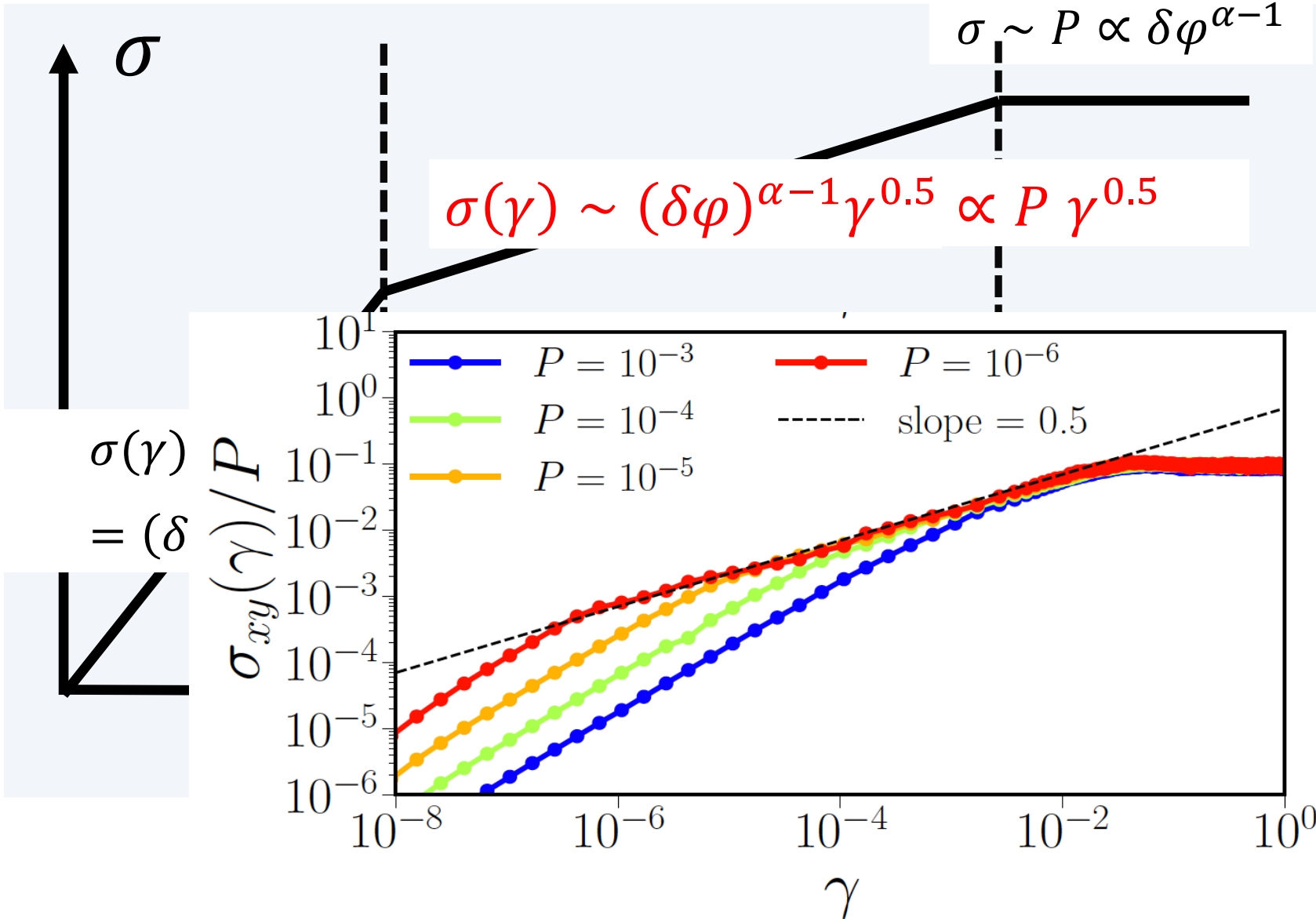
$$\langle \Delta r_{\text{CR}} \rangle \sim 0.1\sigma$$

$$\therefore \gamma_Y \sim 0.1$$



Conclusion: Scaling relations near the jamming transition

Derivation of scaling functions for softening regions



- Intersection of the Softening and Yielding:

$$(\delta\varphi)^a \gamma_Y^b \propto \delta\varphi^{\alpha-1}$$

$$\therefore a = \alpha - 1$$

- Intersection of the elastic and softening

$$(\delta\varphi)^{\alpha-\frac{3}{2}} \gamma_s \propto (\delta\varphi)^{\alpha-1} \gamma_s^b$$

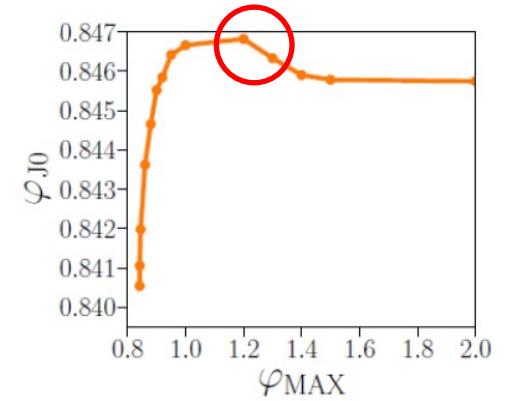
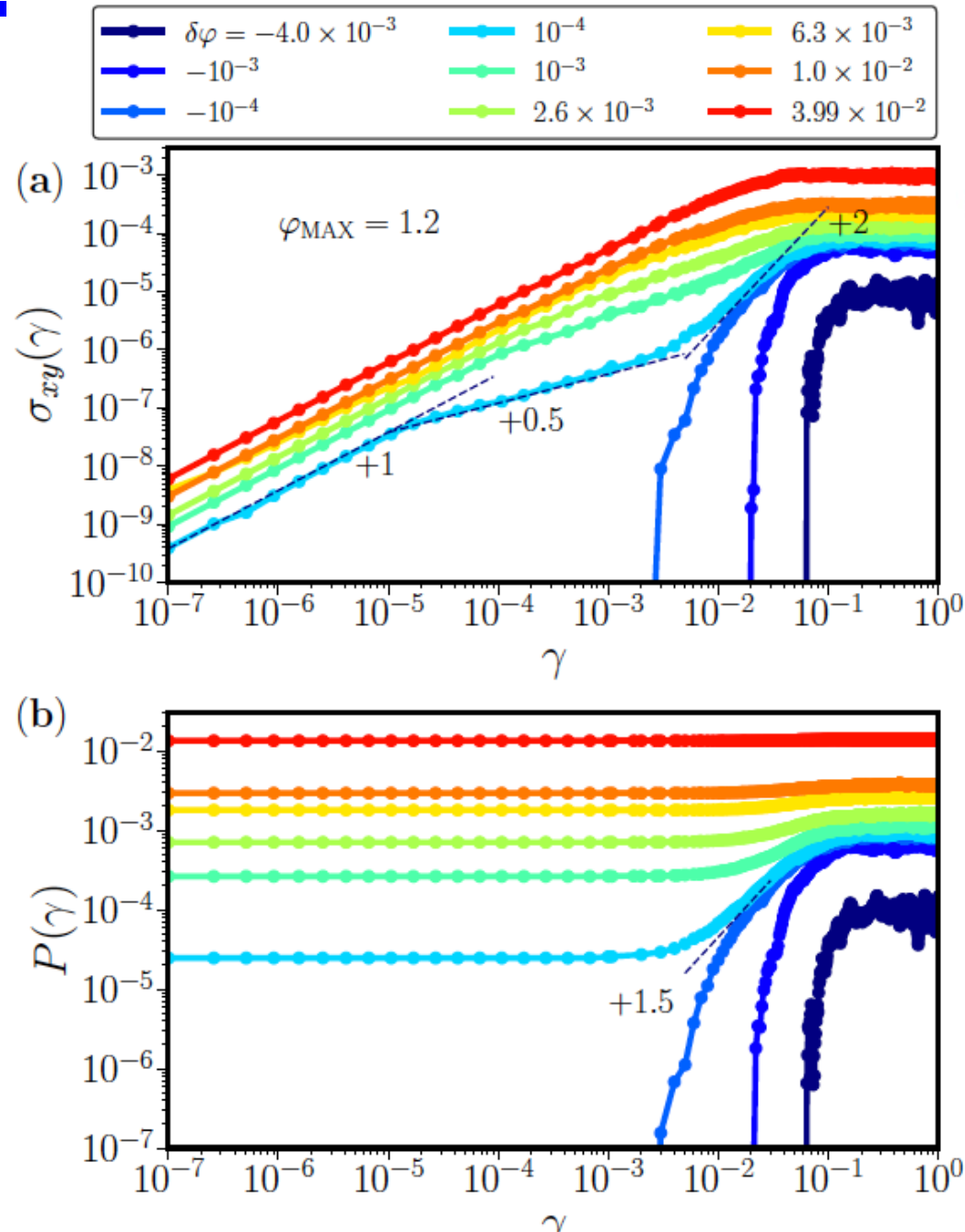
$$\therefore b = \frac{1}{2}$$

Results: Revisit constant volume simulations

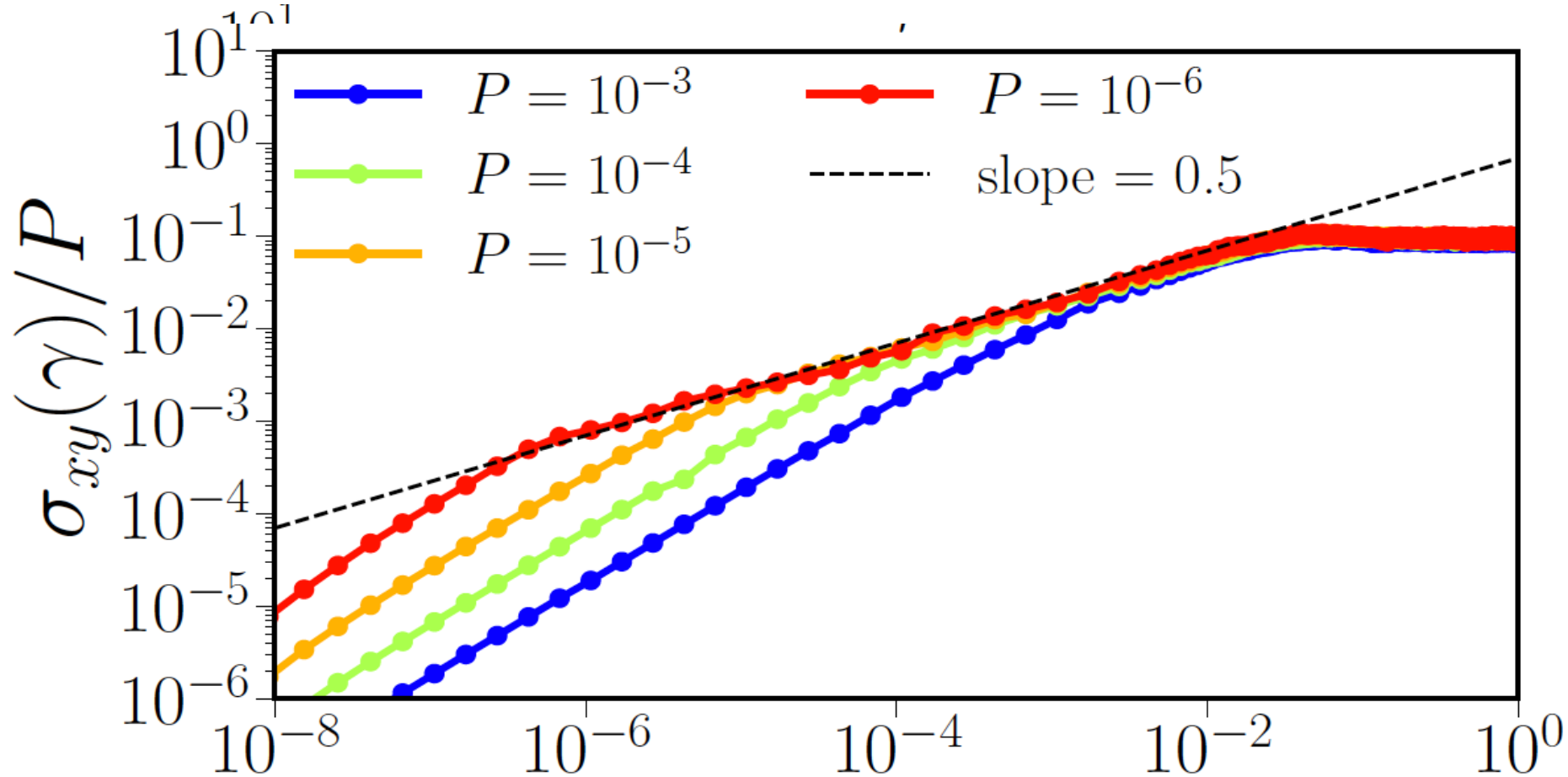
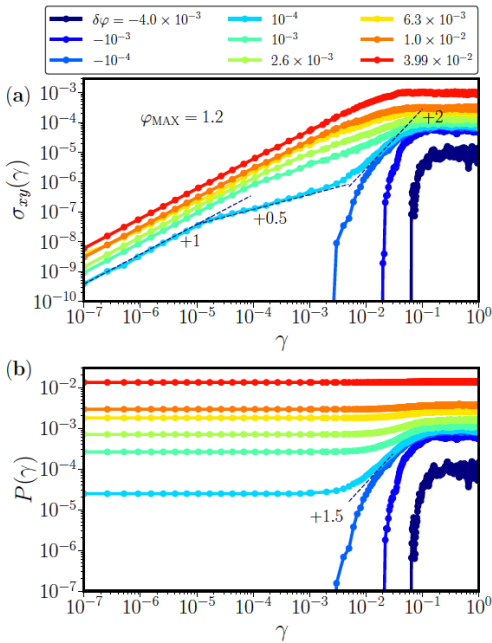
In constant pressure:

- Softening:
 $\sigma(\gamma) \sim P(\gamma) \gamma^{0.5}$
- Yielding:
 $\sigma(\gamma) \sim P(\gamma)$

How about constant volume??



Results: Disentangling of shear hardening, shear jamming and softening in constant volume simulations



Softening:

$$\sigma(\gamma)/P(\gamma) \sim \gamma^{0.5}$$

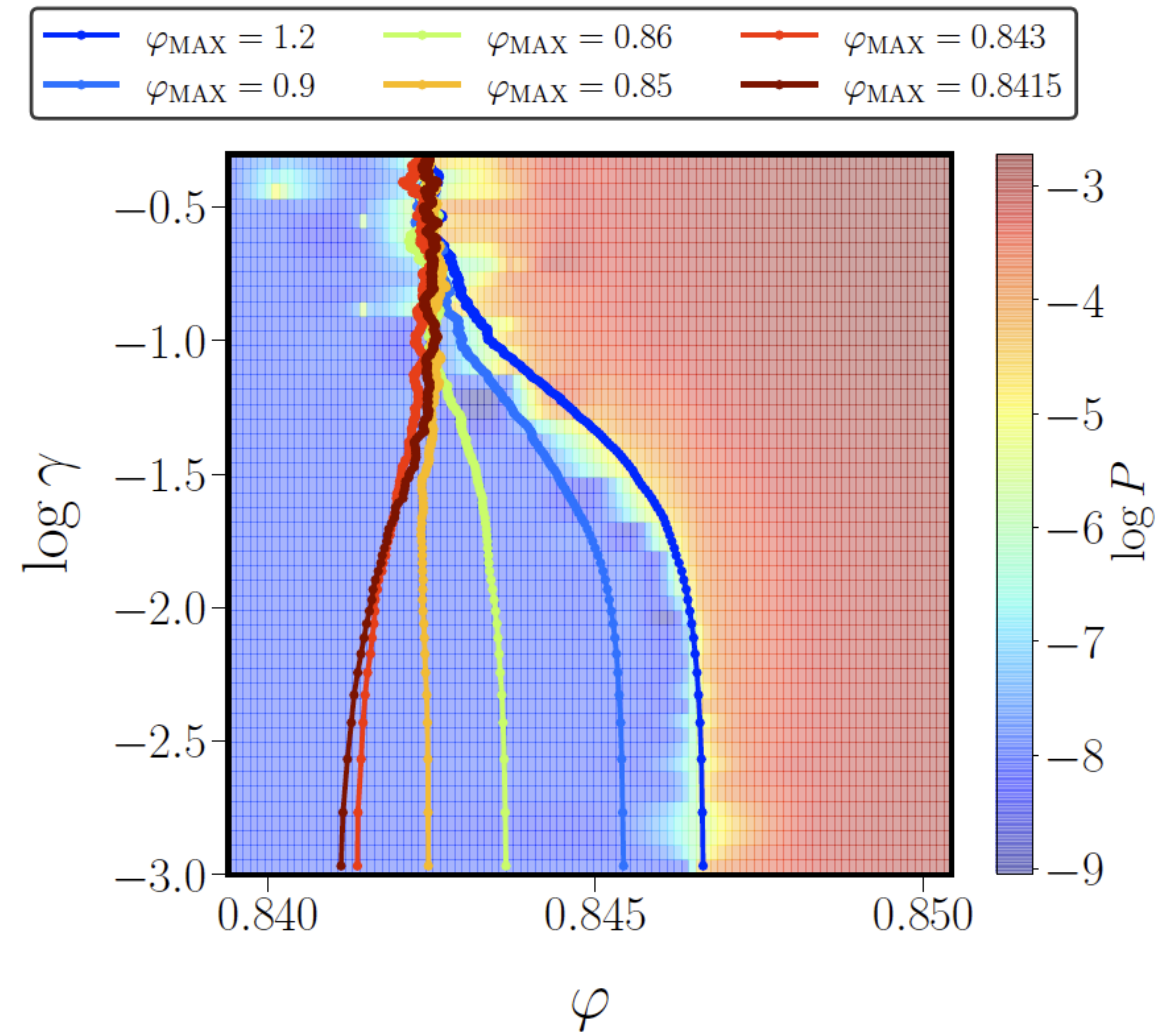
Yielding:

$$\sigma(\gamma)/P(\gamma) \sim \text{const}$$

- Softening exists behind hardening!
- Protocol-independent mechanical response equivalent to constant pressure is obtained.

Conclusions

- Shear jamming / shear hardening/ shear melting are attributed to the change of φ_J .
- Constant pressure simulations are not contaminated by change of φ_J .
 - Wide-range of critical scaling has been obtained regardless of generation protocols of the jamming configurations.
 - Even constant volume, σ/P shows **protocol independent** scaling relations.



Open questions

- Softening and yielding
 - for frictional particle system?
 - at finite shear rate?
 - at unjammed state?
 - with microscopic theoretical arguments?

Thank you for your attention.