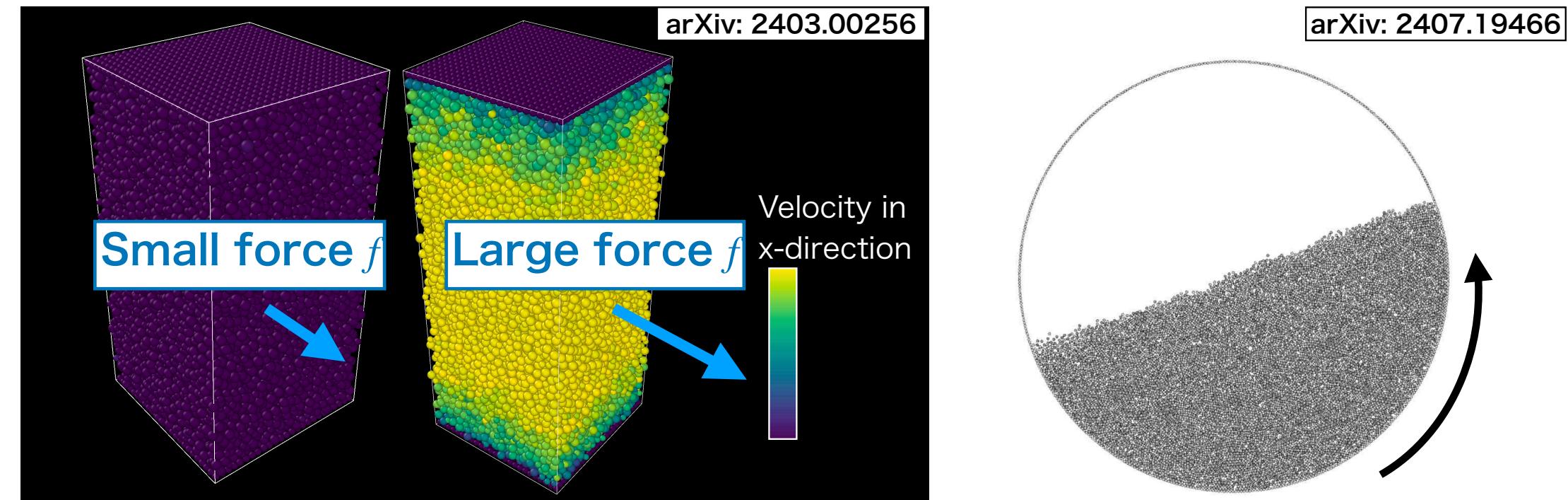


Flow of jammed granular materials

Michio Otsuki (Osaka Univ.)

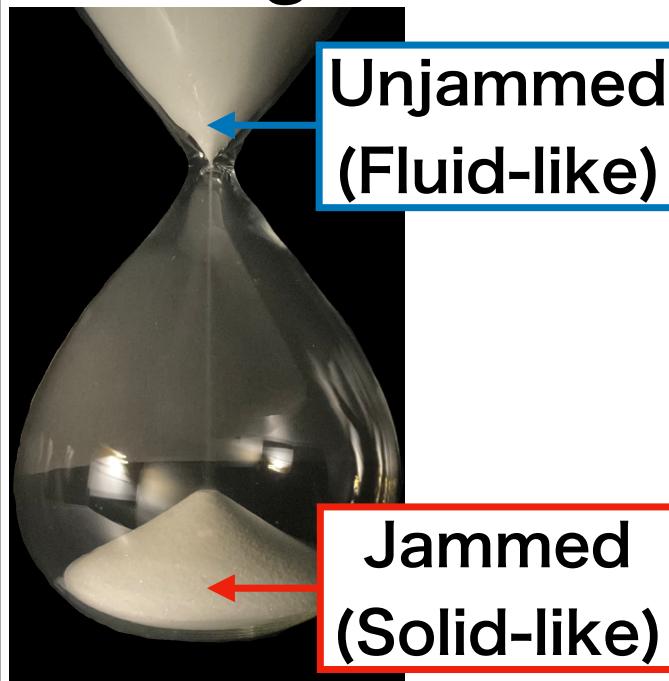


Collaborators: Kiwamu Yoshii, Kenta Hayashi, Hiroki Oba

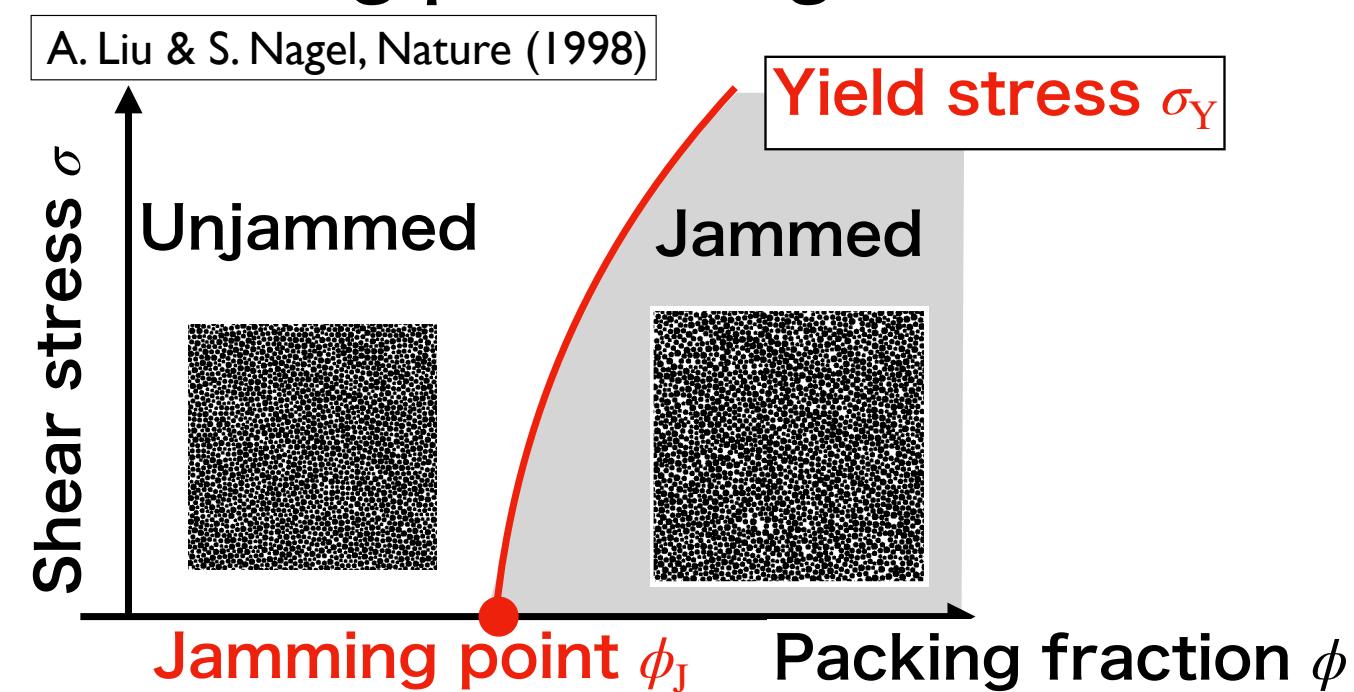
Jamming of granular materials

2/23

► Hourglass



► Jamming phase diagram



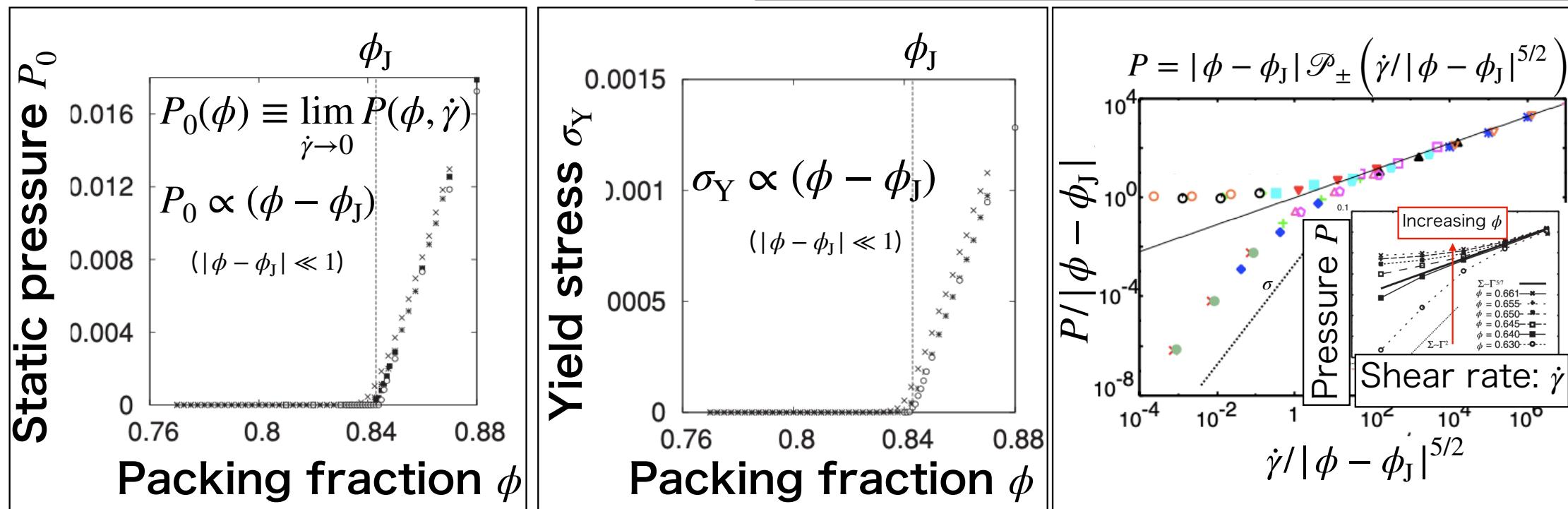
- Unjammed: Fluid-like state with flow ($\phi < \phi_J$ or $\sigma > \sigma_Y$)
- Jammed: Solid-like state without flow ($\phi > \phi_J$ and $\sigma < \sigma_Y$)

Scaling laws near jamming

3/23

- Homogeneous sheared systems with constant ϕ and $\dot{\gamma}$

Otsuki, Hayakawa PRE (2009): Linear repulsive interaction

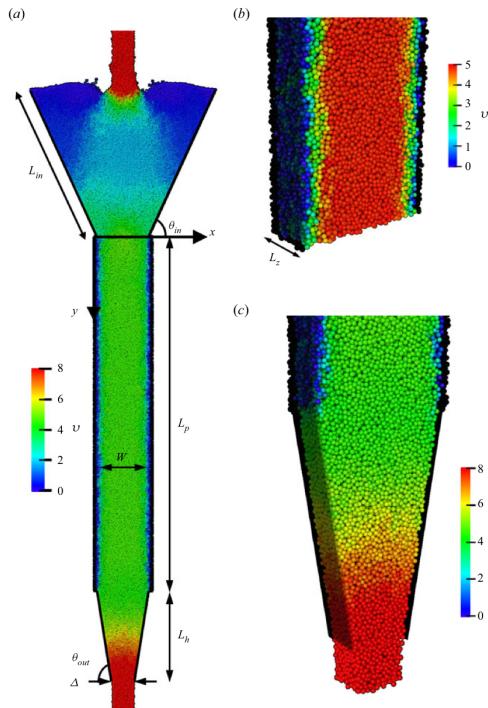


Critical behaviors similar to those for conventional phase transition

Jamming in inhomogeneous systems

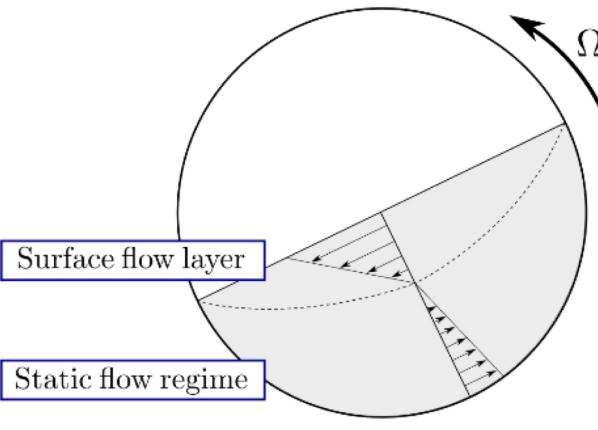
4/23

► Plug region in chute



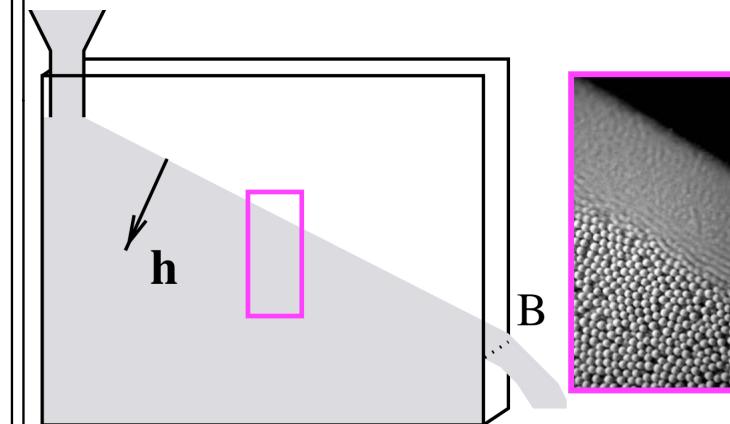
T. Baker et al., J. Fluid Mech. (2022).

► Static region in rotating drum



J. Mellmann , Powder Technol. (2001).

► Static region in sand pile



T. S. Komatsu et al., PRL (2002).

We theoretically derive velocity profile and scaling laws
for inhomogeneous flows.

Table of contents

5/23

1. Introduction
2. Setup (DEM and continuum model)
3. Flow between rough parallel plates
4. Flow in rotating drums
5. Summary

MO, K. Hayashi, and K. Yoshii, arXiv: 2403.00256

H. Oba and MO, arXiv: 2407.19466

DEM and continuum equation

6/23

Discrete Element Method (DEM)

Position r_i , Force F_{ij}

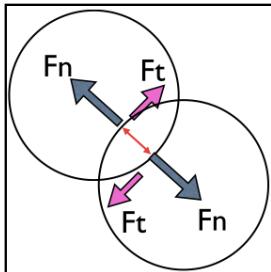
$$m\ddot{r}_i = \sum_j F_{ij}$$

Linear repulsive force F_n

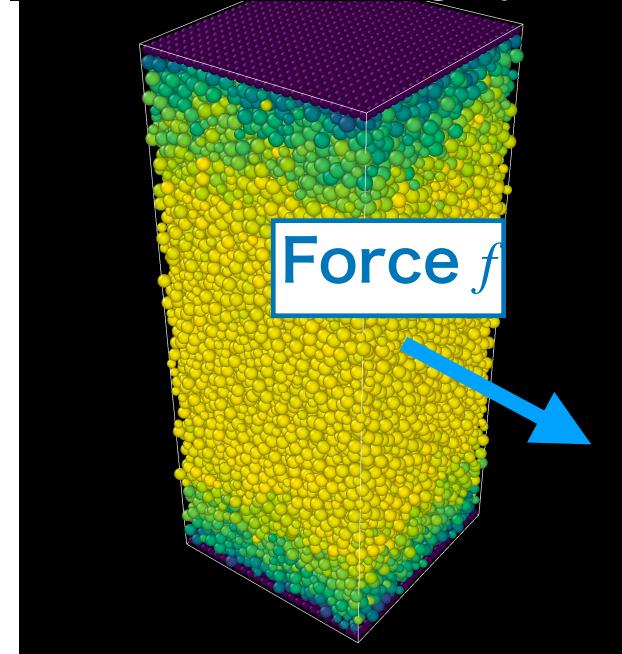
Tangential friction F_t

Coulomb law $|F_t| \leq \mu_p F_n$

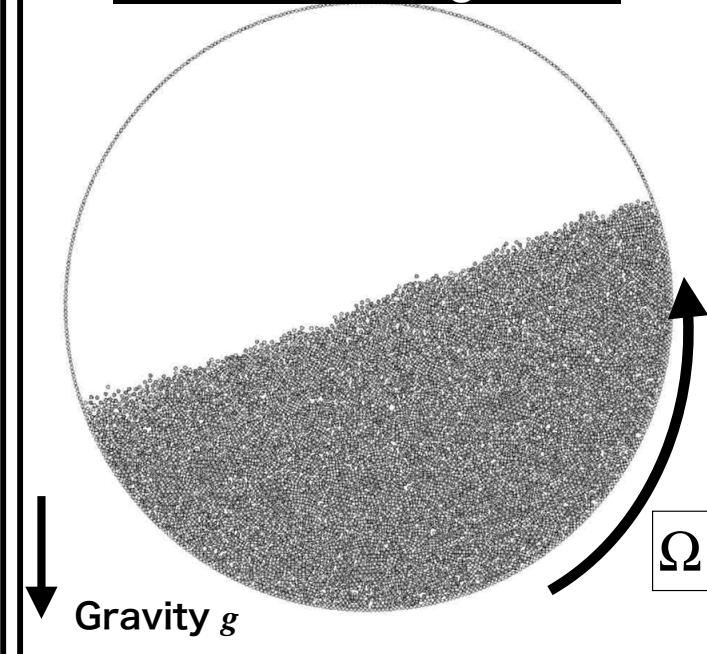
Friction coefficient μ_p



Flow between rough plates



Flow in rotating drum



Continuum equations for theoretical analysis

$$\rho(\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u}) = -\nabla p + \nabla \cdot \boldsymbol{\sigma} + \mathbf{K}$$

Velocity \mathbf{u} , Density ρ , Pressure p , Stress $\boldsymbol{\sigma}$, Body force \mathbf{K}

Constitutive equation for σ : $\mu(I)$ rheology

7/23

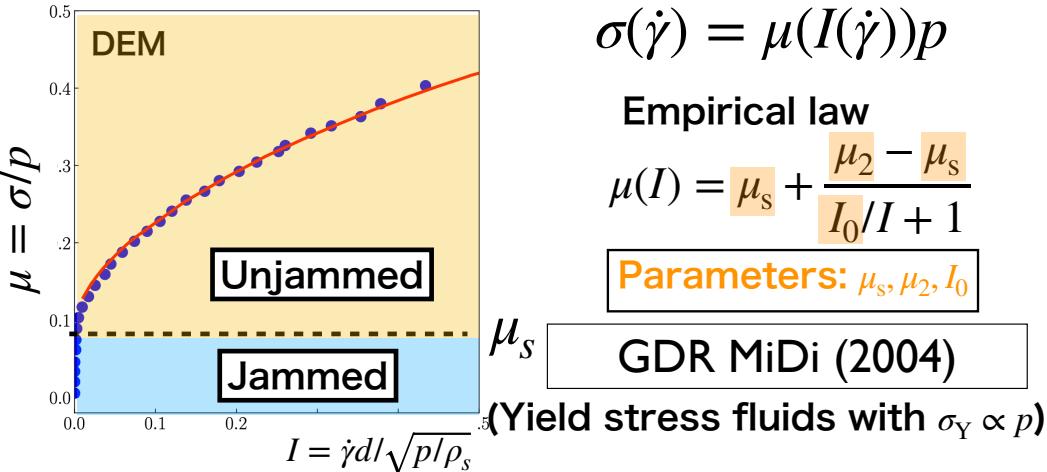
► Simple shear

Bulk friction $\mu = \sigma/p$

Inertia number $I = \dot{\gamma}d/\sqrt{p/\rho_s}$

Shear stress σ , Pressure p , Shear rate $\dot{\gamma}$

Particle diameter d , Particle density ρ_s



Consistent with scaling laws near jamming for $\dot{\gamma} \rightarrow 0$: σ_Y, p

► Generalized form

Stress tensor $\sigma = \mu(I)p \frac{\dot{\gamma}}{|\dot{\gamma}|} = \eta \dot{\gamma}$

Shear rate tensor $\dot{\gamma} = \nabla u + (\nabla u)^T$

$$\mu(I) = \mu_s + \frac{\mu_2 - \mu_s}{I_0/I + 1}, \quad I = |\dot{\gamma}| d / \sqrt{p/\rho_s}$$

$$\text{Viscosity } \eta = \frac{\mu(I)p}{|\dot{\gamma}|}$$

Parameters (μ_s, μ_2, I_0) can be estimated
from DEM under simple shear.

P. Jop et al. Nature (2006)

Table of contents

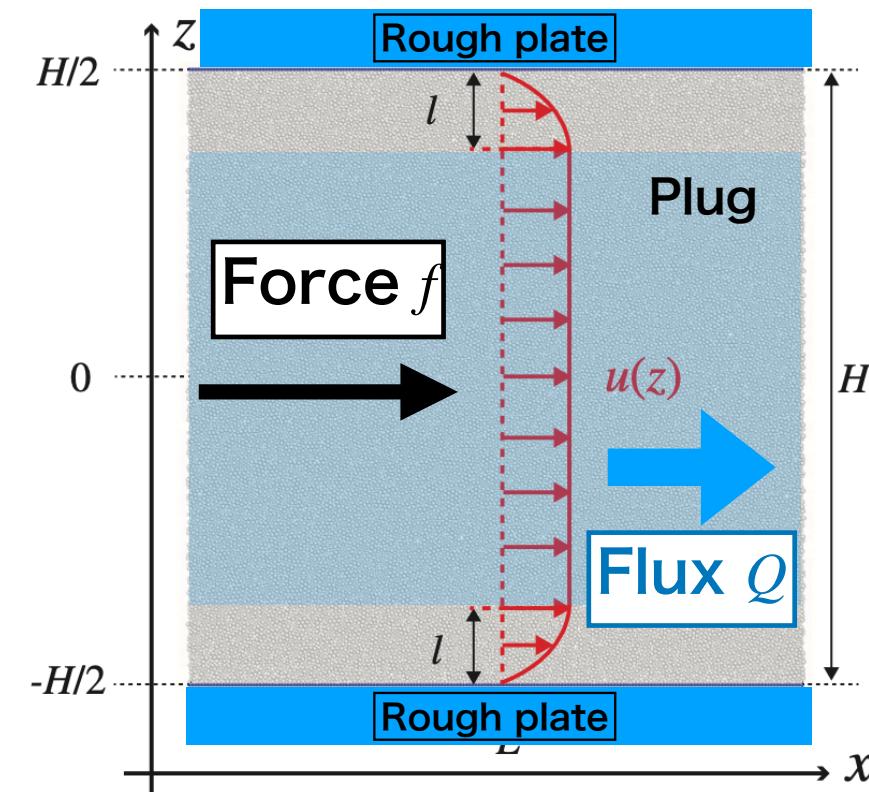
8/23

1. Introduction
2. Setup (DEM and continuum model)
3. **Flow between rough parallel plates**
MO, K. Hayashi, and K. Yoshii, arXiv: 2403.00256
4. Flow in rotating drums
H. Oba and MO, arXiv: 2407.19466
5. Summary

Setup: 2D flow between rough parallel plates

9/23

- Constant volume, periodic B.C along x -direction

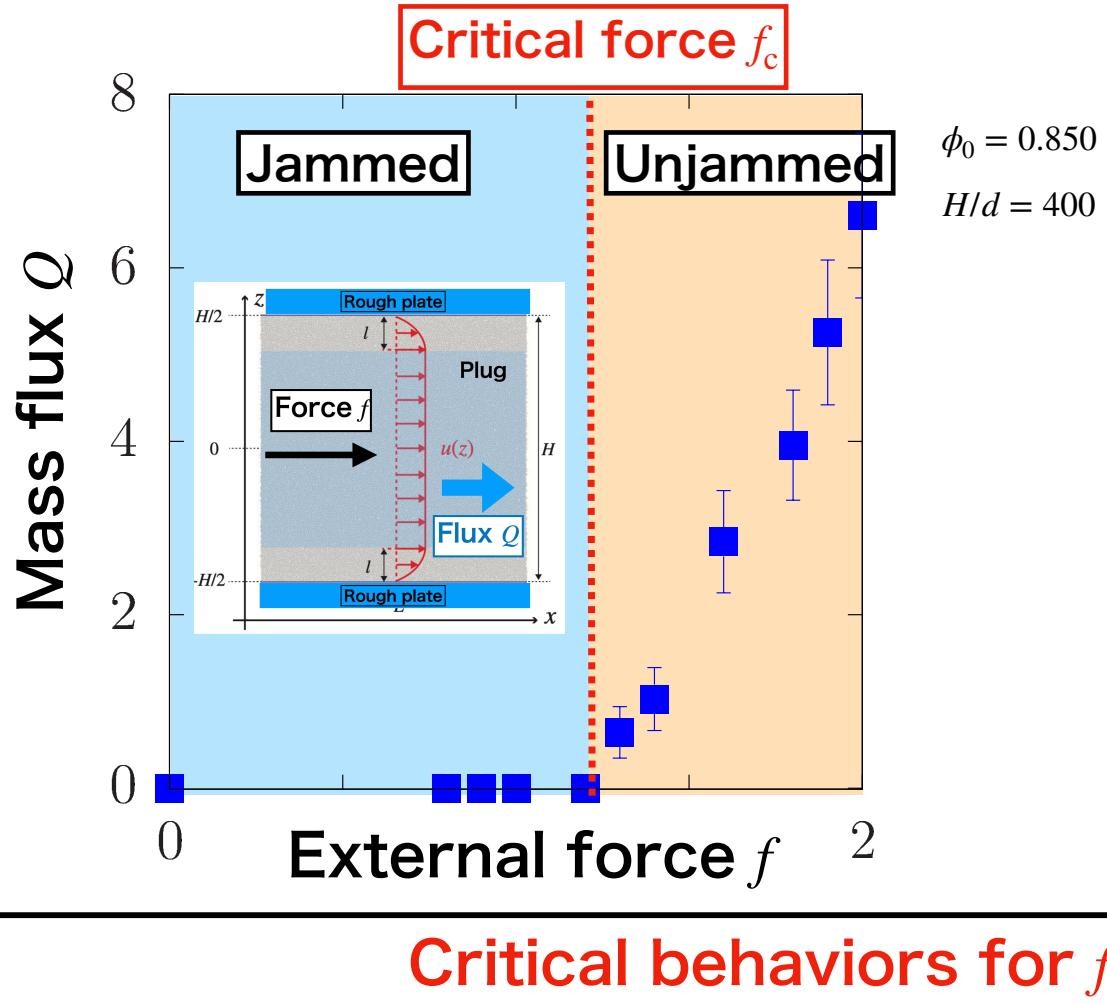


Frictionless N grains
Grain diameter: d
Distance between plates: $H \gg d$
Velocity $u(z)$
Local packing fraction: $\phi(z)$
Average packing fraction: $\phi_0 \geq \phi_J$
External force per unit mass: f

* Constant p , friction, 3D \rightarrow Same scaling law

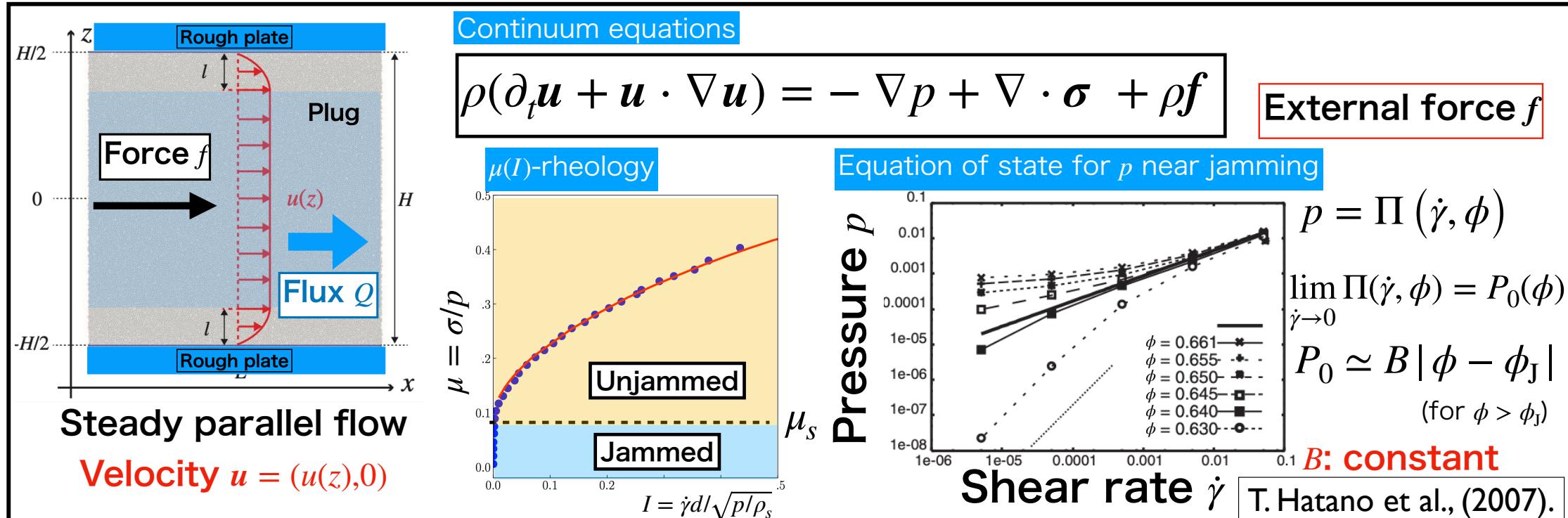
- Solid-like plug region with $\dot{\gamma} = 0$ appears.

Mass flux Q and critical force f_c



Theoretical analysis

arXiv: 2403.00256



↓ Analytical results for $f \sim f_c(\phi_0, H)$, $\phi_0 \sim \phi_J$ using perturbation theory

Critical force

$$f_c(\phi_0, H) = \frac{2\mu_s P_0(\phi_0)}{\rho_s H}, \quad P_0(\phi) = B |\phi - \phi_J| \quad (|\phi - \phi_J| \ll 1)$$

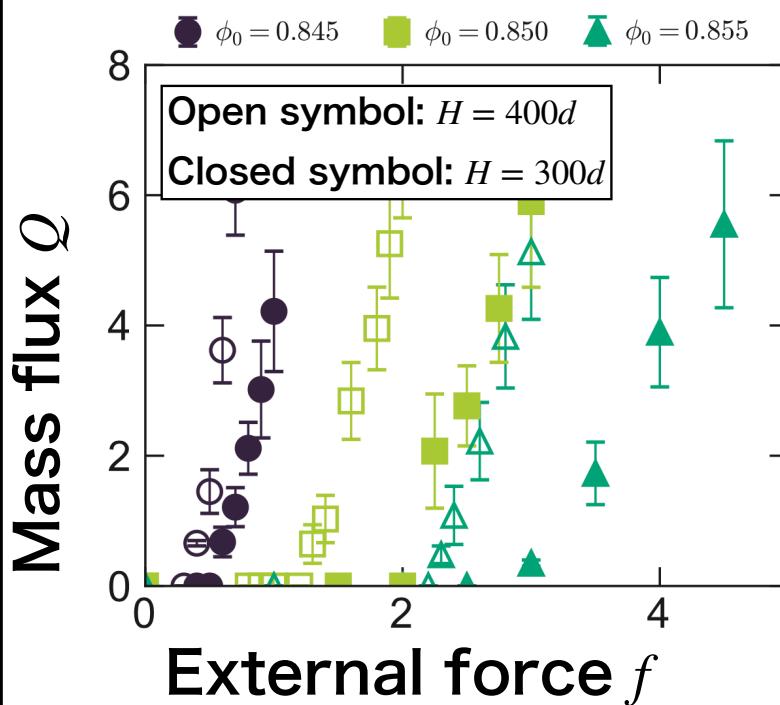
Mass flux

$$Q(f, \phi_0, H) = \frac{\mu_s \phi_0 \sqrt{\rho_s P_0(\phi_0)} H^2}{4bd} \left(\frac{f}{f_c(\phi_0, H)} - 1 \right)^2$$

Scaling laws for critical force f_c

Jammed ($f < f_c$): $Q = 0$

Unjammed ($f > f_c$): $Q > 0$

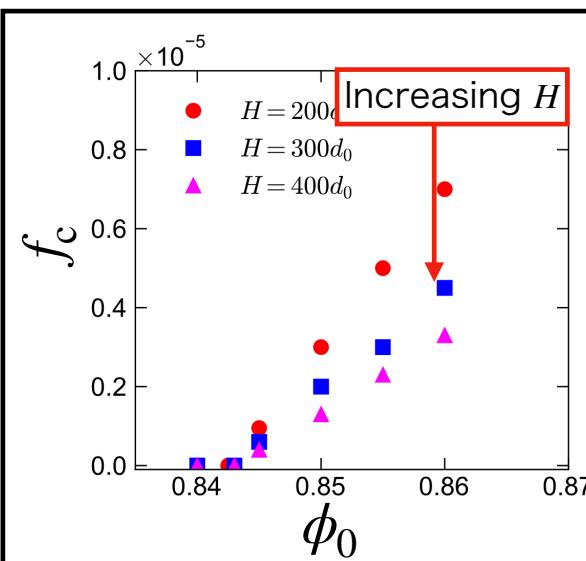


► Critical force ($|\phi - \phi_J| \ll 1$)

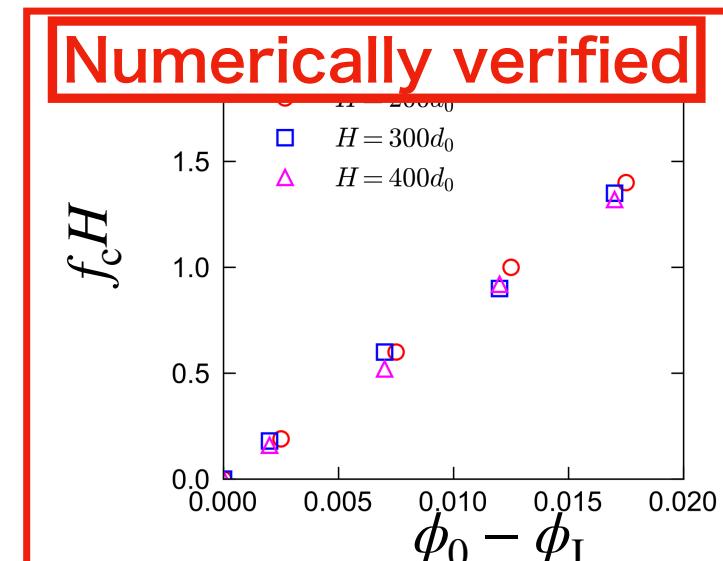
$$f_c(\phi_0, H) = \frac{2\mu_s P_0(\phi_0)}{\rho_s H} = \frac{2\mu_s B |\phi_0 - \phi_J|}{\rho_s H}$$

f_c increases with ϕ_0 . f_c decreases with H .

► Scaling law: $f_c H = \mathcal{F}(\phi_0 - \phi_J)$



Numerically verified



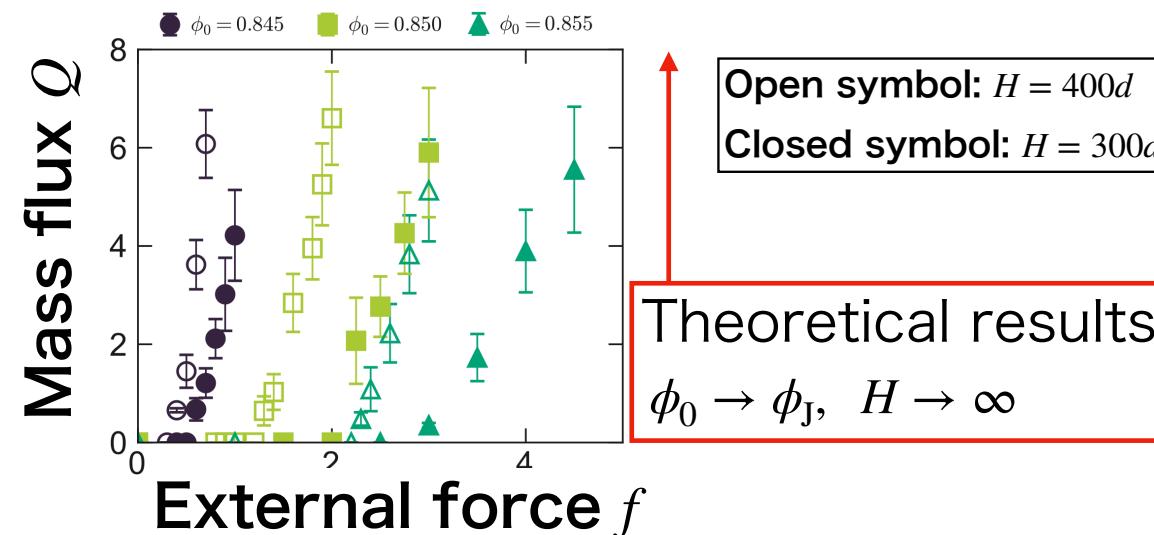
Scaling laws for mass flux Q

13/23

Theoretical results for $f > f_c$

$$Q(f, \phi_0, H) = \frac{\mu_s \phi_0 \sqrt{\rho_s P_0(\phi_0)} H^2}{4bd} \left(\frac{f}{f_c(\phi_0, H)} - 1 \right)^2$$

$$f_c(\phi_0, H) = \frac{2\mu_s P_0(\phi_0)}{\rho_s H}, \quad P_0(\phi) = B |\phi - \phi_J| \quad (|\phi - \phi_J| \ll 1)$$



Critical scaling law

$$\frac{Q}{H^2 \sqrt{|\phi_0 - \phi_J|}} = \mathcal{Q} \left(\frac{fH}{|\phi_0 - \phi_J|} \right)$$

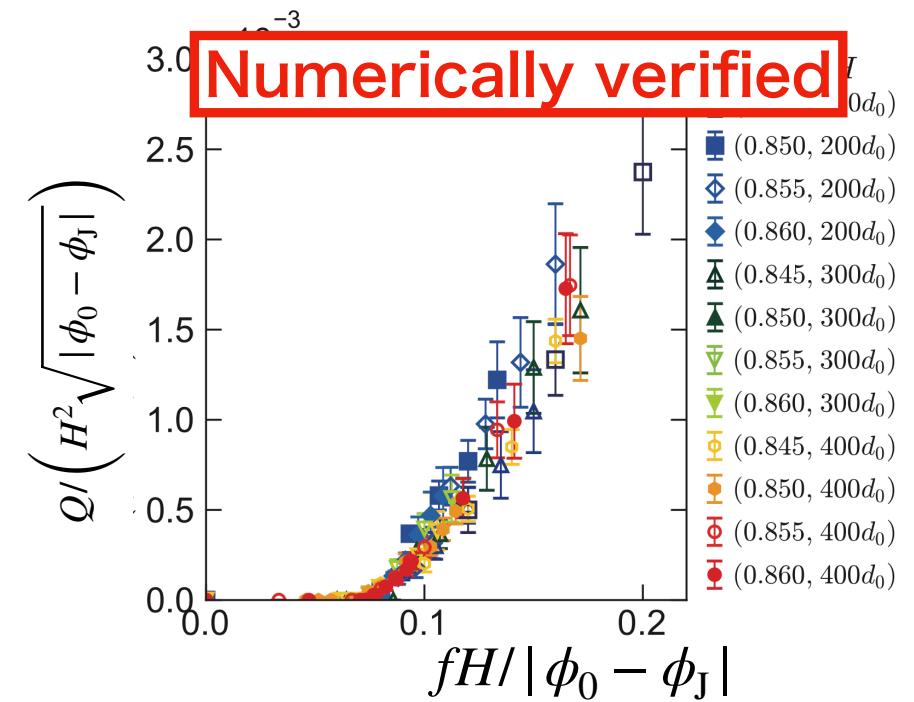


Table of contents

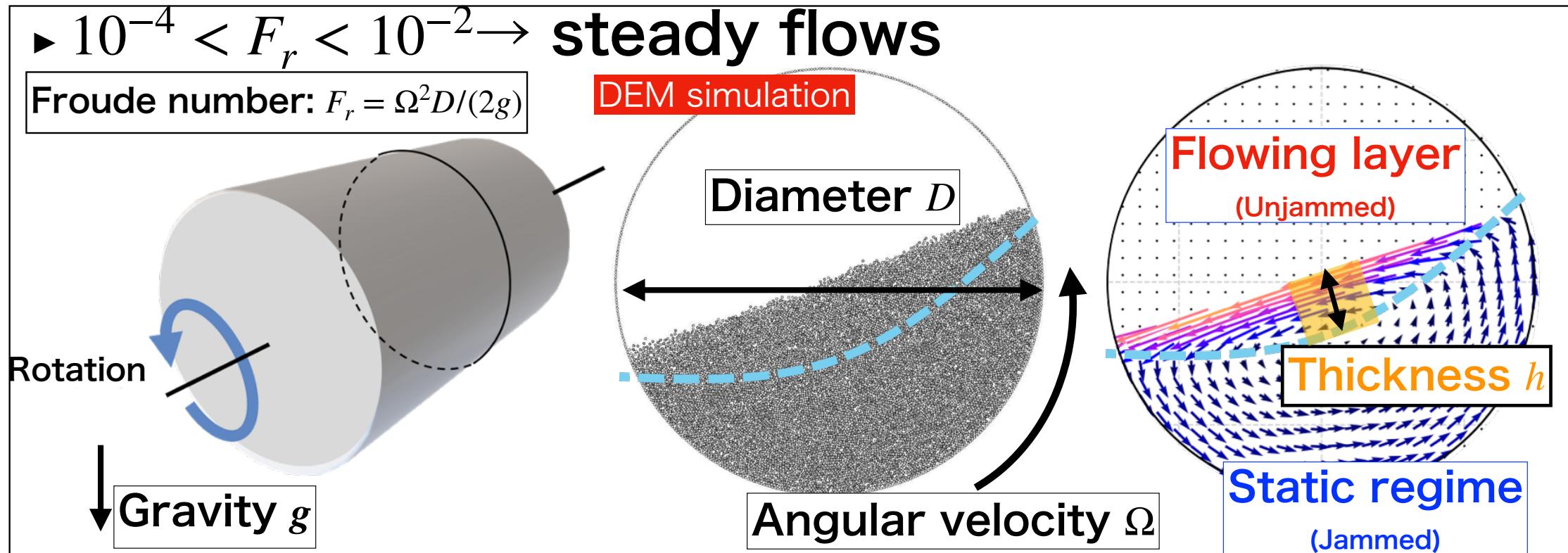
14/23

1. Introduction
2. Setup (DEM and continuum model)
3. Flow between rough parallel plates
4. **Flow in rotating drums**
MO, K. Hayashi, and K. Yoshii, arXiv: 2403.00256
5. Summary

H. Oba and MO, arXiv: 2407.19466

Setup: granular materials in rotating drum

15/23



- Flowing layer (parallel flow) Static regime (rigid rotation)
 - Previous studies : layer thickness $h(\Omega)$????
- D. J. Parker et al.(1997) : $h \sim \text{const.}$, G. Felix et al. (2007) : $h \sim \Omega^\alpha$

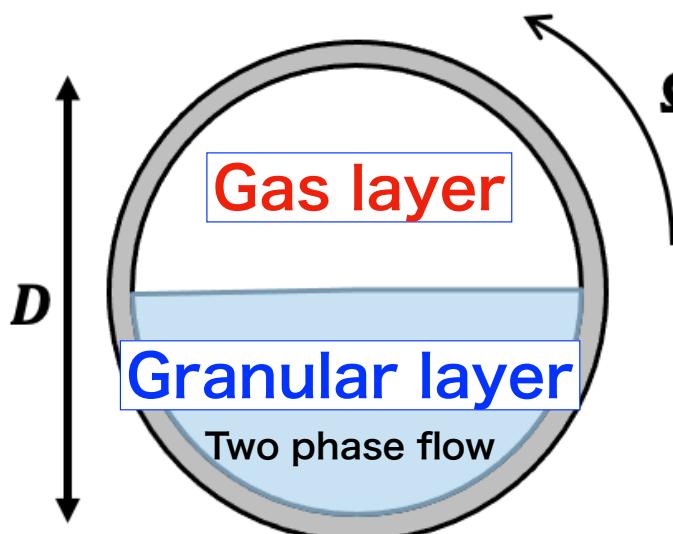
Simulation: 2D-CFD (Computational Fluid Dynamics)

16/23

Time evolution : $\rho(\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u}) = -\nabla p + \nabla \cdot \boldsymbol{\sigma} + \rho g$

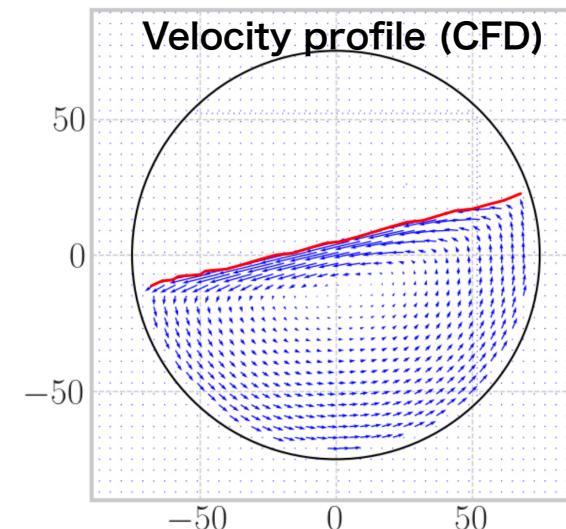
$\mu(I)$ -rheology: $\boldsymbol{\sigma} = \eta \dot{\gamma}$, $\eta = \frac{\mu(I)p}{|\dot{\gamma}|}$, $\mu(I) = \mu_s + \frac{\mu_2 - \mu_s}{I_0/I + 1}$, $I = \frac{|\dot{\gamma}|d}{\sqrt{p/\rho_s}}$

Incompressible condition : $\nabla \cdot \mathbf{u} = 0$ Density ρ , Pressure p , Stress σ , Gravity g



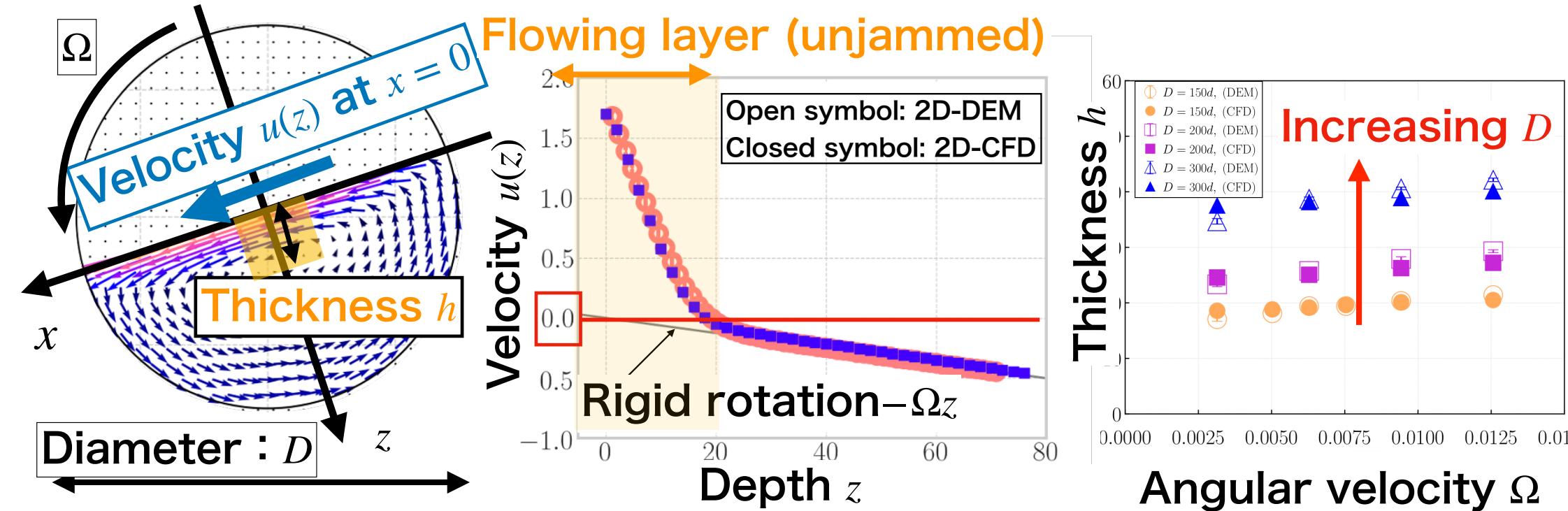
- Free surface: VOF method
- Wall boundary: BDI method

Newtonian fluids: D. Watanabe and S. Goto, (2022)



Velocity $u(z)$ and thickness h

17/23



- DEM and CFD results are quantitatively consistent.
- Flowing layer : $u(z) > 0$, Thickness h : $u(z = h) \simeq 0$
- Thickness h increases with D , and has a slight dependence on Ω .

Nondimensionalized continuum eq.

The continuum model reproduces DEM results.

$$\nabla \cdot \mathbf{u} = 0$$

$$\rho(\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u}) = -\nabla p + \nabla \cdot \boldsymbol{\sigma} + \rho g$$

$$\boldsymbol{\sigma} = \eta \dot{\gamma}, \quad \eta = \frac{\mu(I)p}{|\dot{\gamma}|}, \quad \mu(I) = \mu_s + \frac{\mu_2 - \mu_s}{I_0/I + 1}, \quad I = \frac{|\dot{\gamma}|d}{\sqrt{p/\rho_s}}$$

 Steady flow

\sim : normalized variable

Diameter of drum D ,

Angular velocity Ω ,

Density ρ

$$\nabla \cdot \tilde{\mathbf{u}} = 0$$

Scaled velocity $\tilde{\mathbf{u}}(\tilde{r})$, Scaled position \tilde{r}

$$\tilde{\mathbf{u}} \cdot \tilde{\nabla} \tilde{\mathbf{u}} = -\tilde{\nabla} \tilde{p} + \tilde{\nabla} \cdot (\tilde{\eta} \tilde{\dot{\gamma}}) + (g/\Omega^2 D) \mathbf{e}_z$$

$$\tilde{\eta} = \frac{\mu_s \tilde{p}}{|\tilde{\dot{\gamma}}|} + \frac{(\mu_2 - \mu_s) \tilde{p}(d/D)}{I_0 \sqrt{\phi \tilde{p}} + |\tilde{\dot{\gamma}}|(d/D)}, \quad \tilde{\dot{\gamma}} = \tilde{\nabla} \tilde{\mathbf{u}} + (\tilde{\nabla} \tilde{\mathbf{u}})^T$$

Packing fraction ϕ

Scaling law for velocity profile

19/23

\sim : normalized variable

Diameter of drum D ,

Angular velocity Ω ,

Density ρ , Gravity g

Particle diameter d

$$\nabla \cdot \tilde{\mathbf{u}} = 0$$

Scaled velocity $\tilde{\mathbf{u}}(\tilde{r})$, Scaled position \tilde{r}

$$\tilde{\mathbf{u}} \cdot \tilde{\nabla} \tilde{\mathbf{u}} = -\tilde{\nabla} \tilde{p} + \tilde{\nabla} \cdot (\tilde{\eta} \tilde{\gamma}) + (g/\Omega^2 D) \mathbf{e}_z$$

$$\tilde{\eta} = \frac{\mu_s \tilde{p}}{|\tilde{\gamma}|} + \frac{(\mu_2 - \mu_s) \tilde{p} (d/D)}{I_0 \sqrt{\phi \tilde{p}} + |\tilde{\gamma}| (d/D)}, \quad \tilde{\gamma} = \tilde{\nabla} \tilde{\mathbf{u}} + (\tilde{\nabla} \tilde{\mathbf{u}})^T$$



$$d/D < 0.006 \ll 1$$

$$\nabla \cdot \tilde{\mathbf{u}} = 0, \quad \tilde{\mathbf{u}} \cdot \tilde{\nabla} \tilde{\mathbf{u}} = -\tilde{\nabla} \tilde{p} + \tilde{\nabla} \cdot \left(\frac{\mu_s \tilde{p}}{|\tilde{\gamma}|} \tilde{\gamma} \right) + \frac{g}{\Omega^2 D} \mathbf{e}_z$$

Froude number Fr : $Fr^{-1} = 2g/\Omega^2 D$

External parameter

$$\tilde{\mathbf{u}} = \mathbf{u}/(\Omega D) = V(\tilde{r}; Fr)$$

$u(z)$: Velocity at $x = 0$

$$\tilde{r} = r/D$$

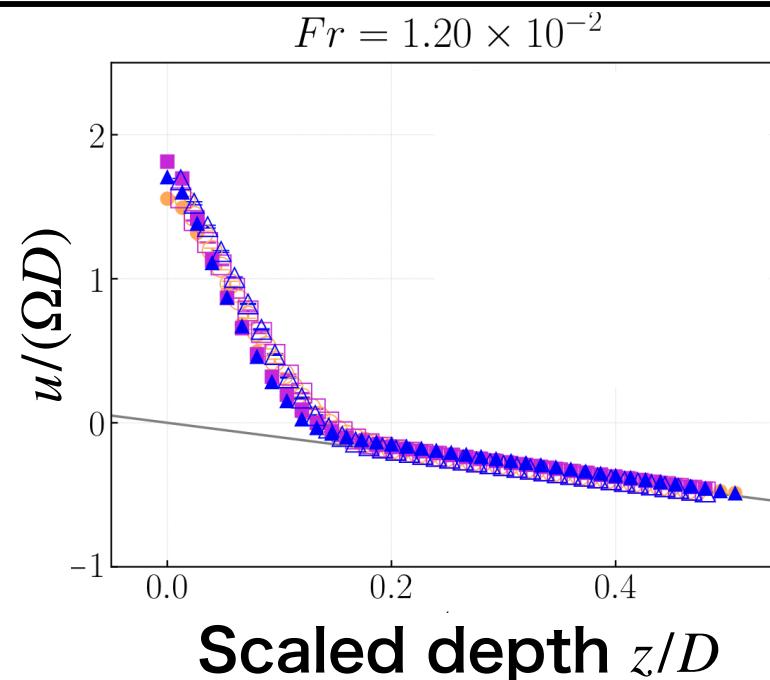
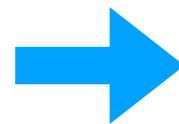
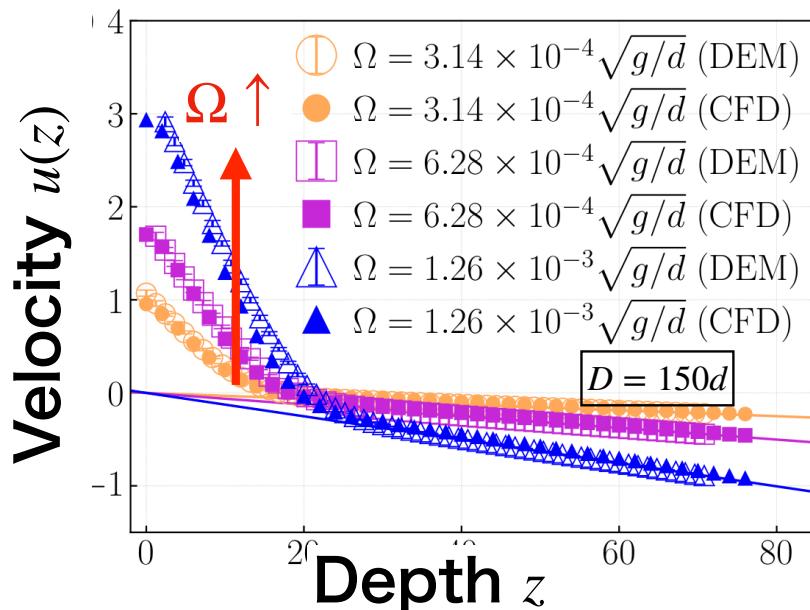
Scaling law : $\frac{u(z; D, \Omega)}{\Omega D} = U\left(\frac{z}{D}; Fr\right)$

Validity of scaling law

20/23

$$\text{Scaling law : } \frac{u(z; D, \Omega)}{\Omega D} = U\left(\frac{z}{D}; Fr\right)$$

Froude number : $Fr = \Omega^2 D / (2g)$



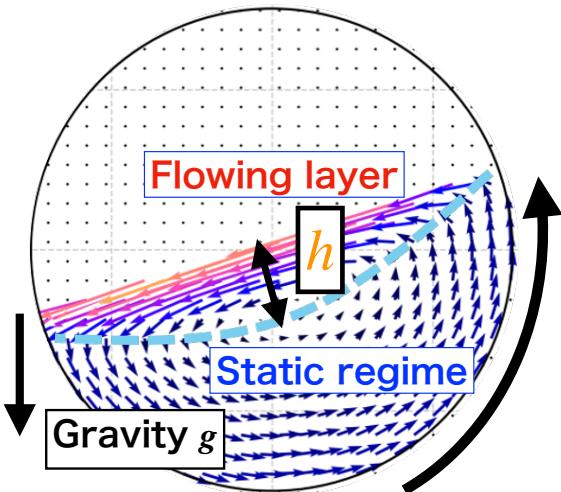
- The scaling law is confirmed by simulations.

Scaling law for thickness of flowing layer

21/23

Scaling law : $\frac{u(z; D, \Omega)}{\Omega D} = U\left(\frac{z}{D}; Fr\right)$

Thickness h : $u(z = h) \simeq 0$



$$\frac{h(D, \Omega)}{D} = \mathcal{H}(Fr)$$

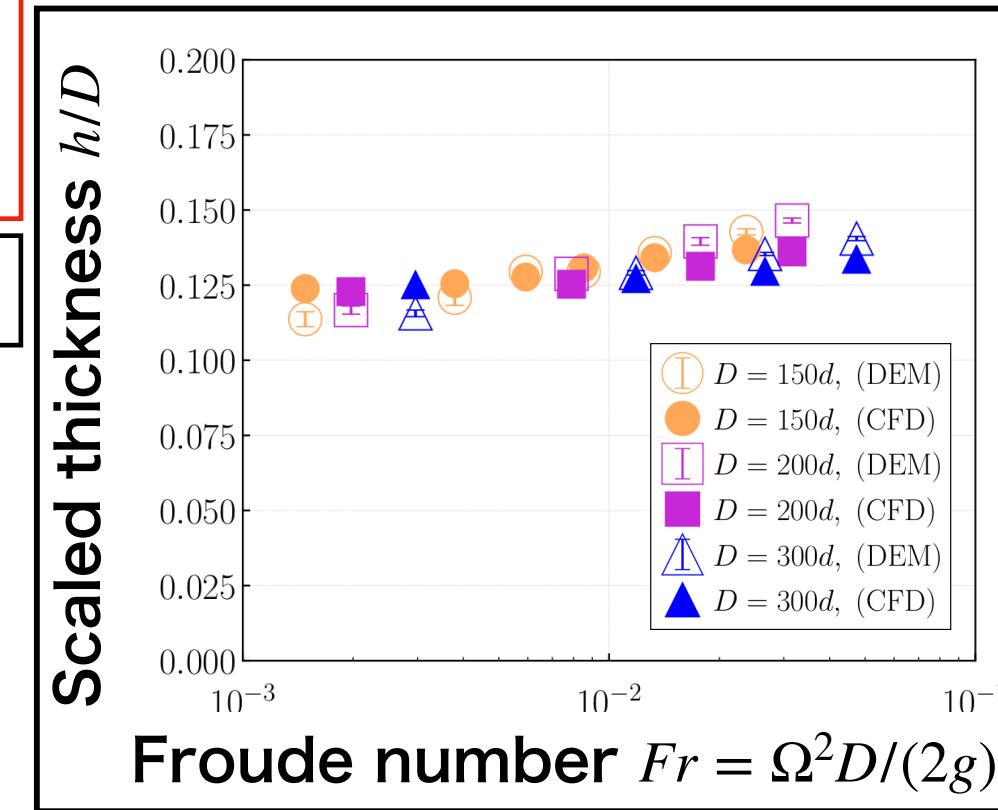
$$\mathcal{H}(Fr) \simeq \tilde{H}^{(0)} + Fr\tilde{H}^{(1)}$$

Derived from conservation of flux

$$Fr = \Omega^2 D / (2g)$$

► The scaling law for h is verified.

► h is proportional to D and slowly increases with Ω .



Froude number $Fr = \Omega^2 D / (2g)$

cf. long drum exp. [D. J. Parker et al. (1997)]

Table of contents

22/23

1. Introduction
2. Setup (DEM and continuum model)
3. Flow between rough parallel plates
MO, K. Hayashi, and K. Yoshii, arXiv: 2403.00256
4. Flow in rotating drums
H. Oba and MO, arXiv: 2407.19466
5. Summary

Summary

23/23

- **Topic:** Flow of jammed granular materials
- **Theoretical analysis:** Continuum eq. with $\mu(I)$ -rheology
- **Result 1:** Scaling law for mass flux in parallel flows. arXiv: 2403.00256
- **Result 2:** Scaling law for flowing layer thickness h in rotating drums. arXiv: 2407.19466

